

层流边界层方程的近似分析解*

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摘 要

文献[1]引用压力梯度作为新的自变量以代替通常的纵坐标 x , 从而将经典的边界层方程变为新的形式。在此基础上, 文献[1]用图解法求定任一截面处的摩擦应力因子。

本文仍然采用文献[1]的变量置换, 但用级数法求得了层流边界层方程的一级近似分析解, 并得到了计算摩擦应力因子的公式(4.13)。对于主函数中不含常数项的一类流动说, 本文求得的摩擦应力因子和文献[1]的结果十分符合; 对于主函数中含有常数项的另一类流动, 文中作了进一步的简化, 求得的摩擦应力因子和文献[1]的结果相比较, 误差也低于 10%。

关键词 层流边界层 压力梯度 摩擦应力因子

一、方程的变换和级数解法的提出

平面定常不可压缩层流边界层方程为

$$\left. \begin{aligned} u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= U \frac{dU}{dx} + \nu \frac{\partial^2 u}{\partial y^2} \\ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} &= 0 \end{aligned} \right\} \quad (1.1)$$

边界条件为

$$\left. \begin{aligned} y=0 \text{ 时, } u=v &= 0 \\ y \rightarrow \infty \text{ 时, } u &\rightarrow U(x) \end{aligned} \right\} \quad (1.2)$$

式中 u, v ——流速沿 x, y 轴的投影,

ν ——运动粘性系数,

$U(x)$ ——主流的速度。

按照[1], 引用新的独立变量

$$\xi = \frac{x}{U} \frac{dU}{dx}, \quad \eta = y \sqrt{\frac{U}{\nu x}} \quad (1.3)$$

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并令流函数为

$$\psi = \sqrt{\nu U x} f(\xi, \eta) \quad (1.4)$$

将式(1.3)及(1.4)代入式(1.1)及(1.2), 文献[1]得到了关于未知函数 $f(\xi, \eta)$ 的偏微分方程。求其精确的分析解是十分困难的。文献[1]在此基础上用图解法求定摩擦应力因子。

我们试图用级数法求此问题的近似分析解。

联合 ξ 及 η 的新的相似参量是没有的。但考虑到在边界层中, 物理量沿流动方向 (x 方向) 的变化远较垂直于流动方向的变化⁽³⁾小, 因而我们仿效文献[2]的思想, 为了得到收敛很快的级数解, 我们令

$$f = \sum_{n=0}^{\infty} \xi^n f_n(\eta) \quad (1.5)$$

则有

$$\left. \begin{aligned} \psi &= \sqrt{\nu U x} \sum_{n=0}^{\infty} \xi^n f_n(\eta) \\ u &= \frac{\partial \psi}{\partial y} = U \sum_{n=0}^{\infty} \xi^n f'_n \\ \frac{\partial u}{\partial y} &= U \sqrt{\frac{U}{\nu x}} \sum_{n=0}^{\infty} \xi^n f''_n, \quad \frac{\partial^2 u}{\partial y^2} = \frac{U^2}{\nu x} \sum_{n=0}^{\infty} \xi^n f'''_n \\ \frac{\partial u}{\partial x} &= U \left[\sum_{n=0}^{\infty} \left(f'_n n \xi^{n-1} \frac{d\xi}{dx} + \xi^n f''_n y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2}\right) x^{-3/2} \right. \right. \\ &\quad \left. \left. + \xi^n f''_n y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right) \right] + \frac{dU}{dx} \sum_{n=0}^{\infty} \xi^n f'_n \\ v &= -\frac{\partial \psi}{\partial x} = -\sqrt{\nu U x} \left[\sum_{n=0}^{\infty} \left(f_n \cdot n \xi^{n-1} \frac{d\xi}{dx} \right. \right. \\ &\quad \left. \left. + \xi^n f'_n y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2}\right) x^{-3/2} + \xi^n f'_n y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \right. \right. \\ &\quad \left. \left. \cdot \frac{dU}{dx} \right) \right] - \sum_{n=0}^{\infty} \xi^n f_n(\eta) \left[\frac{1}{2} \sqrt{\nu x} U^{-1/2} \frac{dU}{dx} \right. \\ &\quad \left. + \frac{1}{2} \sqrt{\nu x} x^{-1/2} \right] \end{aligned} \right\} (1.6)$$

将式(1.6)代入式(1.1)及(1.2)得

$$U \sum_{n=0}^{\infty} \xi^n f'_n \left\{ U \left[\sum_{n=0}^{\infty} f'_n n \xi^{n-1} \frac{d\xi}{dx} + \xi^n f''_n y \sqrt{\frac{U}{\nu}} \right. \right.$$

$$\begin{aligned}
& \cdot \left(-\frac{1}{2} x^{-3/2} + \xi^n f_n'' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right) + \frac{dU}{dx} \\
& \cdot \sum_{n=0}^{\infty} \xi^n f_n'' + \left\{ -\sqrt{\nu U x} \left[\sum_{n=0}^{\infty} \left(f_n \cdot n \xi^{n-1} \frac{d\xi}{dx} + \xi^n \right. \right. \right. \\
& \cdot f_n' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} + \xi^n f_n' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \cdot \frac{dU}{dx} \right) \Big] \\
& \left. \left. - \sum_{n=0}^{\infty} \xi^n f_n(\eta) \left[\frac{1}{2} \sqrt{\nu x} U^{-1/2} \frac{dU}{dx} + \frac{1}{2} \sqrt{\nu U} x^{-1/2} \right] \right\} \\
& \cdot U \sqrt{\frac{U}{\nu x}} \sum_{n=0}^{\infty} \xi^n f_n'' = U \frac{dU}{dx} + \nu \cdot \frac{U^2}{\nu x} \sum_{n=0}^{\infty} \xi^n f_n''
\end{aligned} \tag{1.7}$$

边界条件为

$$\left. \begin{aligned} f_0'(0) &= 0, f_n(0) = 0 \\ f_0'(\infty) &= 1, [f_n'(\infty)]_{n \neq 0} = 0 \end{aligned} \right\} \tag{1.8}$$

我们只限于求式(1.7)及(1.8)的一级近似解, 故只取 $n=0$ 及 $n=1$, 而抛弃 $n>1$ 的一切项。于是, 方程(1.7)变为

$$\begin{aligned}
& U f_0' \left\{ U \left[\left(f_0'' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} + f_0'' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \right. \right. \right. \right. \\
& \cdot \frac{dU}{dx} \Big] + \frac{dU}{dx} f_0' \Big\} + \left\{ -\sqrt{\nu U x} \left[f_0' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} \right. \right. \right. \\
& + f_0' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \Big] - f_0 \left[\sqrt{\nu x} \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right. \\
& \left. \left. + \frac{1}{2} \sqrt{\nu U} x^{-1/2} \right] \right\} U \sqrt{\frac{U}{\nu x}} f_0'' + U \xi f_1' \left\{ U \left[f_1' \frac{d\xi}{dx} \right. \right. \\
& \left. \left. + \xi f_1'' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} + \xi f_1'' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right) \right] \right. \\
& \left. + \frac{dU}{dx} \xi f_1' \right\} + \left\{ -\sqrt{\nu U x} \left[f_1 \frac{d\xi}{dx} + \xi f_1' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} \right. \right. \right. \\
& \left. \left. + \xi f_1' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right] - \xi f_1 \left[\sqrt{\nu x} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right. \right. \\
& \left. \left. + \sqrt{\nu U} \cdot \frac{1}{2} x^{-1/2} \right] \right\} U \sqrt{\frac{U}{\nu x}} \xi f_1'' + \dots = U \frac{dU}{dx} \\
& + \frac{U^2}{x} f_0'' + \xi f_1'' \frac{U^2}{x} + \dots
\end{aligned}$$

各项均乘以 x/U^2 , 并化简得

$$\begin{aligned}
& -f_0 f_0'' \left(\frac{1}{2} \frac{x}{U} \frac{dU}{dx} + \frac{1}{2} \right) + f_0'^2 \frac{x}{U} \frac{dU}{dx} + \xi x f_1' \\
& \cdot \left[f_1' \frac{d\xi}{dx} + \xi f_1'' y \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} x^{-3/2} + \xi f_1'' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \right. \right.
\end{aligned}$$

$$\begin{aligned} & \cdot \frac{dU}{dx} \Big] + \frac{x}{U} \frac{dU}{dx} \xi^2 f_1'^2 - x \xi f_1'' \left[f_1 \frac{d\xi}{dx} + \xi f_1' y \right. \\ & \cdot \left. \sqrt{\frac{U}{\nu}} \left(-\frac{1}{2} \right) x^{-3/2} + \xi f_1' y \sqrt{\frac{1}{\nu x}} \cdot \frac{1}{2} U^{-1/2} \frac{dU}{dx} \right] - \xi^2 f_1 f_1'' \\ & \cdot \frac{x}{U} \frac{dU}{dx} - \xi^2 f_1 f_1'' \cdot \frac{1}{2} + \dots = \frac{x}{U} \frac{dU}{dx} + f_0''' + \xi f_1''' + \dots \end{aligned}$$

即

$$\begin{aligned} & -f_0 f_0'' \frac{1}{2} (\xi + 1) + f_0' \xi + x \frac{d\xi}{dx} (\xi f_1'^2 - \xi f_1 f_1'') - \frac{1}{2} \xi^2 \\ & \cdot \eta f_1' f_1'' + \frac{1}{2} \eta \xi^3 f_1' f_1'' + \xi^3 f_1'^2 + \frac{1}{2} \xi^2 \eta f_1' f_1'' - \frac{1}{2} \xi^3 \eta \\ & \cdot f_1' f_1'' - \xi^3 f_1 f_1'' - \frac{1}{2} \xi^2 f_1 f_1'' + \dots = \xi + f_0''' + \xi f_1''' + \dots \end{aligned} \quad (1.9)$$

合并含 ξ^0 的各项及含 ξ 的各项, 并分别令其系数为 0, 得

$$-\frac{1}{2} f_0 f_0'' = f_0''' \quad (1.10)$$

$$-\frac{1}{2} f_0 f_0'' + f_0'^2 - 1 - f_1''' + \left[x \frac{d\xi}{dx} \right]_c (f_1'^2 - f_1 f_1'') = 0 \quad (1.11)$$

式中

$[x d\xi/dx]_c$ 表示只取乘积 $x \cdot d\xi/dx$ 的常数项, 如果无常数项, 则 $[x d\xi/dx]_c = 0$. 一级近似时, 边界条件(1.8)则为

$$\left. \begin{aligned} f_0'(0) = f_1'(0) = 0, \quad f_0(0) = f_1(0) = 0 \\ f_0'(\infty) = 1, \quad f_1'(\infty) = 0 \end{aligned} \right\} \quad (1.12)$$

二、零级近似解

求零级近似解时, 问题归结为求解式(1.10)及(1.12), 这个问题的精确的分析解是难于求得的, 勃拉休斯(Blasius)首先找到了这个问题的数值解, 通常称为勃拉休斯解.

卡门和波尔郝森则提出了以动量方程为基础的层流边界层方程的近似积分法. 这种方法归结为将边界层各截面上未知的实际速度曲线 $u(x, y)$ 用四次抛物线族^[4]

$$\frac{u}{U} = \frac{12 + \lambda}{6} \cdot \frac{y}{\delta} - \frac{\lambda}{2} \left(\frac{y}{\delta} \right)^2 - \frac{4 - \lambda}{2} \left(\frac{y}{\delta} \right)^3 + \frac{6 - \lambda}{6} \left(\frac{y}{\delta} \right)^4 \quad (2.1)$$

式中

$$\lambda = U' \delta^2 / \nu \quad (2.2)$$

δ ——边界层的厚度. 将式(2.1)代入卡门动量方程, 波尔郝森得到了决定 δ 的微分方程. 对于平板, $U' = 0$, $\lambda = 0$, 可求得

$$\delta = 5.83 \sqrt{\frac{\nu x}{U}} \quad (2.3)$$

将式(2.3)及 $\lambda = 0$, $\eta = y \sqrt{U/(\nu x)}$ 代入式(2.1)得

$$U = \frac{2}{5.83} \eta - \frac{2}{5.83^3} \eta^3 + \frac{1}{5.83^4} \eta^4 \quad (2.4)$$

式(1.6)中, 对于平板, 应取 $n=0$, 而有

$$u = U f'_0 \quad (2.5)$$

比较式(2.4)及(2.5), 我们得

$$f'_0 = \frac{2}{5.83} \eta - \frac{2}{5.83^3} \eta^3 + \frac{1}{5.83^4} \eta^4 \quad (2.6)$$

积分一次, 并利用边界条件 $f_0(0)=0$, 得

$$f_0 = \frac{1}{5.83} \eta^2 - \frac{1}{5.83^3 \times 2} \eta^4 + \frac{1}{5.83^4 \times 5} \eta^5 \quad (2.7)$$

将式(2.6)微分一次得

$$f''_0 = \frac{2}{5.83} - \frac{6}{5.83^3} \eta^2 + \frac{4}{5.83^4} \eta^3 \quad (2.8)$$

式(2.7)实质上是式(1.10)及(1.12)的近似分析解。为了估计式(2.7)的精确程度, 我们把式(2.6)~(2.8)和勃拉休斯的准确解(数值解)做了比较(表1)。

表1

$\eta = y \sqrt{\frac{U}{\nu x}}$	f_0		f'_0		f''_0	
	近似式(2.7)	准确	近似式(2.6)	准确	近似式(2.8)	准确
0.2	0.006857	0.00664	0.06853	0.06641	0.3419	0.33199
0.4	0.02732	0.02656	0.1366	0.13277	0.3384	0.33147

文献[5]中的表8~3也指出了波尔郝森近似法的平板问题的准确程度。

看来, 用波尔郝森法求得的式(1.10)的近似分析解式(2.7), 其准确度是相当高的, 把它做为本文的零级近似解应该是合理的。

于是, 我们得到了问题的零级近似解式(2.5)~(2.8)。

三、 $\zeta = x \cdot d\xi/dx$ 中无常数项时, 问题的一级近似解

现设 $\zeta = x \cdot d\xi/dx$ 中无常数项, 即

$$\left[x \frac{d\xi}{dx} \right]_0 = 0 \quad (3.1)$$

式中 $\zeta = x \cdot d\xi/dx$ 文献[1]称为主函数, 它反映各种边界层的主流速度 U 的特点。

满足条件(3.1)时, 一级近似方程(1.11)简化成为

$$f_1''' = -\frac{1}{2} f_0 f_0'' + f_0'^2 - 1 \quad (3.2)$$

式中, 为了避免和下一节的符号相混淆, 我们把 f_1''' 改写成为 f_1'' 。

将式(2.6)~(2.8)代入上式得

$$f_1'' = -\frac{1}{2} \left(\frac{1}{5.83} \eta^2 - \frac{1}{5.83^3 \times 2} \eta^4 + \frac{1}{5.83^4 \times 5} \eta^5 \right) \\ \times \left(\frac{2}{5.83} - \frac{6}{5.83^3} \eta^2 + \frac{4}{5.83^4} \eta^3 \right) + \frac{1}{5.83^2} \left(2\eta - \frac{2}{5.83^2} \eta^3 \right)$$

$$\begin{aligned}
& + \frac{1}{5.83^3} \eta^4)^2 - 1 = \eta^8 \left(\frac{1}{5.83^8} - \frac{1}{2} \times \frac{1}{5.83^4 \times 5} \times \frac{4}{5.83^4} \right) \\
& + \eta^7 \left(\frac{1}{5.83^3 \times 4} \times \frac{4}{5.83^4} + \frac{1}{5.83^4 \times 10} \times \frac{6}{5.83^8} - \frac{4}{5.83^7} \right) \\
& + \eta^6 \left(\frac{-1}{5.83^3 \times 4} \times \frac{6}{5.83^8} + \frac{1}{5.83^2} \times \frac{4}{5.83^4} \right) \\
& + \eta^5 \left(-\frac{2}{5.83^6} - \frac{1}{5.83^6 \times 5} + \frac{4}{5.83^6} \right) + \eta^4 \left(\frac{3}{5.83^4} \right. \\
& \left. + \frac{1}{5.83^4 \times 2} - \frac{8}{5.83^4} \right) + \eta^2 \left(-\frac{1}{5.83^2} + \frac{4}{5.83^2} \right) - 1
\end{aligned}$$

即

$$\begin{aligned}
f_{10}'' = & \frac{3}{5} \left(\frac{\eta}{5.83} \right)^8 - \frac{12}{5} \left(\frac{\eta}{5.83} \right)^7 + \frac{5}{2} \left(\frac{\eta}{5.83} \right)^6 + \frac{9}{5} \left(\frac{\eta}{5.83} \right)^5 \\
& - \frac{9}{2} \left(\frac{\eta}{5.83} \right)^4 + 3 \left(\frac{\eta}{5.83} \right)^2 - 1
\end{aligned} \quad (3.3)$$

积分一次得

$$\begin{aligned}
f_{10}' = & 5.83 \left[\frac{1}{15} \left(\frac{\eta}{5.83} \right)^9 - \frac{3}{10} \left(\frac{\eta}{5.83} \right)^8 + \frac{5}{14} \left(\frac{\eta}{5.83} \right)^7 + \frac{3}{10} \left(\frac{\eta}{5.83} \right)^6 \right. \\
& \left. - \frac{9}{10} \left(\frac{\eta}{5.83} \right)^5 + \left(\frac{\eta}{5.83} \right)^3 - \frac{\eta}{5.83} \right] + C_1
\end{aligned} \quad (3.4)$$

式中 C_1 为积分常数。再积分一次，并利用边界条件 $f_{10}'(0)=0$ ，得

$$\begin{aligned}
f_{10}' = & 5.83^2 \left[\frac{1}{150} \left(\frac{\eta}{5.83} \right)^{10} - \frac{1}{30} \left(\frac{\eta}{5.83} \right)^9 \right. \\
& + \frac{5}{112} \left(\frac{\eta}{5.83} \right)^8 + \frac{3}{70} \left(\frac{\eta}{5.83} \right)^7 - \frac{3}{20} \left(\frac{\eta}{5.83} \right)^6 \\
& \left. + \frac{1}{4} \left(\frac{\eta}{5.83} \right)^4 - \frac{1}{2} \left(\frac{\eta}{5.83} \right)^2 \right] + C_1 \eta
\end{aligned} \quad (3.5)$$

现决定积分常数 C_1 。我们求得的分析解式(3.3)~(3.5)是以近似解式(2.6)~(2.8)为基础的。由式(1.3)及(2.3)知，当 $y=\delta$ 时， $\eta=5.83$ 。因此，边界条件应改为

$$\left. \begin{aligned}
f_0'(0) = f_{10}'(0) = 0, \quad f_0(0) = f_{10}(0) = 0 \\
f_0'(5.83) = 1, \quad f_{10}'(5.83) = 0
\end{aligned} \right\} \quad (3.6)$$

于是，将 $f_{10}'(5.83)=0$ 代入式(3.5)得

$$C_1 \times 5.83 = -5.83^2 \left(\frac{1}{150} - \frac{1}{30} + \frac{5}{112} + \frac{3}{70} - \frac{3}{20} + \frac{1}{4} - \frac{1}{2} \right)$$

故

$$C_1 = 1.9773 \quad (3.7)$$

将式(3.5)再积分一次，并利用边界条件 $f_{10}(0)=0$ ，得

$$f_{10} = 5.83^3 \left[\frac{1}{1650} \left(\frac{\eta}{5.83} \right)^{11} - \frac{1}{300} \left(\frac{\eta}{5.83} \right)^{10} + \frac{5}{1008} \left(\frac{\eta}{5.83} \right)^9 \right.$$

$$\begin{aligned}
 & + \frac{3}{560} \left(\frac{\eta}{5.83} \right)^6 - \frac{3}{140} \left(\frac{\eta}{5.83} \right)^7 + \frac{1}{20} \left(\frac{\eta}{5.83} \right)^8 \\
 & - \frac{1}{6} \left(\frac{\eta}{5.83} \right)^9 \Big] + 0.9887\eta^2 \quad (3.8)
 \end{aligned}$$

$$\left. \begin{aligned}
 f &= f_0 + \xi f_{10} \\
 f' &= f'_0 + \xi f'_{10} \\
 f'' &= f''_0 + \xi f''_{10}
 \end{aligned} \right\} \quad (3.9)$$

于是, 式(3.8)~(3.9)便构成了问题的一级近似解。它们只适合于主流的速度符合 $\xi = x \cdot d\xi/dx$ 中无常数项的情形。

现求摩擦应力。按照[1], 摩擦应力的无因次形式为

$$C_f = \frac{\tau_0}{\rho U^2} = \sqrt{\frac{\nu}{xU}} \varphi \quad (3.10)$$

式中 φ 为摩擦应力因子,

$$\tau_0 = \mu \frac{\partial u}{\partial y} \Big|_{y=0} \quad (3.11)$$

式中 μ 为流体的粘性系数。将式(1.6)代入, 得一级近似下

$$C_f = \frac{\mu}{\rho U^2} U \sqrt{\frac{U}{\nu x}} \sum_{n=0}^{\infty} \xi^n f''_n(0) = \sqrt{\frac{\nu}{xU}} \sum_{n=0}^{\infty} \xi^n f''_n(0)$$

故由式(3.10)得

$$\varphi = \sum_{n=0}^{\infty} \xi^n f''_n(0) \quad (3.12)$$

一级近似时,

$$\varphi = f''_0(0) + \xi f''_{10}(0) \quad (3.13)$$

由式(2.8)得

$$f''_0(0) = 2/5.83 = 0.3431 \quad (3.14)$$

由式(3.8)得

$$f''_{10}(0) = 1.9773 \quad (3.15)$$

将式(3.14)及(3.15)代入式(3.13), 最后得一级近似下计算摩擦应力因子的公式为

$$\varphi = 0.3431 + 1.9773\xi \quad (3.16)$$

式(3.16)适于一切主函数 $\xi = x d\xi/dx$ 中无常数项, 即 $[x d\xi/dx]_0 = 0$ 的情形。

例1 当主流速度为 $U = 1 - x$ 时, 则有

$$\xi = -\frac{x}{1-x}, \quad \xi = x \cdot \frac{d\xi}{dx} = \xi - \xi^2, \quad \text{即} \left[x \frac{d\xi}{dx} \right]_0 = 0,$$

故式(3.16)适用。

图1表示一级近似下, 例1的摩擦应力因子随纵坐标 x 变化的情形。实曲线表示准确值^[1], 虚线表示本文的结果, 即式(3.16)。由图1可见, 二者十分符合。只是在分离点(φ

$=0$ 附近,二者才出现明显的差异。

当 $\varphi=0$ 时,流动发生分离。由式(3.16)

得

$$\xi = -0.1735$$

由

$$-0.1735 = -x/(1-x)$$

得

$$x = 0.1479$$

准确值为^[1] $x = 0.12$, 误差为23.5%

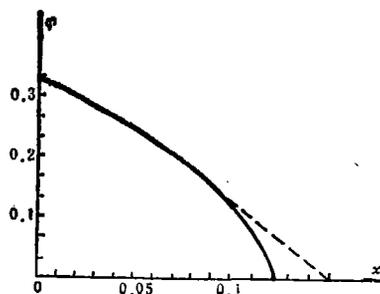


图 1

四、主函数 $\zeta = x \cdot d\xi/dx$ 为任意时的一级近似解

当 $[x \cdot d\xi/dx]_c = A \neq 0$ 时,我们需要求解式(1.11),而不是求解式(3.2)。边界条件则仍然是式(3.6)。

将式(2.6)~(2.8)代入式(1.11),用电子计算机不难求得式(1.11)及(3.6)的数值解。

我们来求它们的近似分析解。为此,需要将式(1.11)做进一步的简化。

1. 按照[1],对于两种不同的流动说,只要二者的 ζ 值和 ξ 值彼此各各相等,则 φ 值亦相同,即是说, φ 值是 ξ 和 ζ 的函数。

但由本文的式(3.16)知,如果 $\zeta = x \cdot d\xi/dx$ 中无常数项,即 $[x \cdot d\xi/dx]_c = 0$ 时,则一级近似时, φ 值只是 ξ 的函数,而与 ζ 无关。例如,对于流动 $U = x \cdot \exp[-x]$ 说, $\zeta = -\xi$;对于流动 $U = 1-x$ 说, $\zeta = \xi - \xi^2$ 。这两种流动的 ζ 值不相同,但因 $[x \cdot d\xi/dx]_c = 0$,故这两种流动有相同的 φ 值。(当二者的 ξ 值相等时)

另一方面,对于 $\zeta = [x d\xi/dx]_c = A \neq 0$ 的一类流动说,则由式(1.11)知,函数 f_1 与 A 有关,因而 φ 值也与 A 有关。即 φ 值与 ζ 有关。

一级近似时,对于不同类型的流动, φ 值的计算结果存在上述的如此本质的差异,是不能被允许的。因此,我们只能得结论,一级近似时,式(1.11)的左边最后一项 $[x d\xi/dx]_c \times (f_1'^2 - f_1 f_1'')$ 很小。

2. 由于 $A(f_1'^2 - f_1 f_1'')$ 很小,按照M. E. Швец的逐步逼近法^[7],求式(1.11)的零级近似解时,我们令 $A(f_1'^2 - f_1 f_1'') = 0$,于是式(1.11)变为式(3.2),而可求得 $f_1 = f_{10}$ 。求式(1.11)的一级近似解时,令 $A(f_1'^2 - f_1 f_1'') = A(f_{10}'^2 - f_{10} f_{10}'')$,式(1.11)简化成为

$$-f_0 f_0''/2 + f_0'^2 - 1 - f_1'' + A(f_{10}'^2 - f_{10} f_{10}'') = 0 \quad (4.1)$$

式中 $f_0, f_0', f_{10}, f_{10}'$,及 f_{10}'' 分别由式(2.6)~(2.8)及(3.4)~(3.8)决定。由于求解式(4.1)仍然很繁难,我们将进一步简化式(4.1)。

按照文献[6],求解弗克纳-斯肯方程

$$f''' + ff'' + \beta(1 - f'^2) = 0$$

时,令

$$f = \sum_{n=0}^{\infty} \beta^n f_n$$

这实质上是认为许多实际流动均接近于绕平板的流动,即认为

$$1 - f'^2 \approx 0$$

基于这种思想, 我们认为

$$f_0'^2 - 1 \approx 0$$

由式(3.2)知, 此时

$$f_{10}''' \approx -f_0 f_0''/2$$

再结合式(1.10)得

$$f_{10}''' \approx f_0'' \quad (4.2)$$

故得

$$f_{10}'' = f_0'' + C_2$$

式中 C_2 为积分常数。由于 f_{10}'' 及 f_0'' 均无任何边界条件约束, 所以, 我们假设

$$f_{10}'' \approx f_0'' \quad (4.3)$$

至于 f_{10}' 及 f_0' , 则因 $f_{10}'(5.83) = 0$, $f_0'(5.83) = 1$, 且 $f_0'^2 - 1 \approx 0$, 故

$$f_{10}' \approx f_0' \quad (4.4)$$

由于

$$\left. \begin{aligned} f_{10} &= f_{10}(0) + f_{10}'(0)\eta + \frac{1}{2}f_{10}''(0)\eta^2 + \dots \\ f_0 &= f_0(0) + f_0'(0)\eta + \frac{1}{2}f_0''(0)\eta^2 + \dots \end{aligned} \right\} \quad (4.5)$$

由式(3.6)有

$$f_{10}(0) = f_0(0) = 0; \quad f_{10}'(0) = f_0'(0) = 0$$

故当 η 很小时, 由上式及式(4.3)及(4.5)可得

$$f_0 \approx f_{10}$$

我们假设在整个边界层内, 有

$$f_{10} \approx f_0 \quad (4.6)$$

由式(4.3)及(4.6)得

$$f_{10}'' f_{10} \approx f_0'' f_0 \quad (4.7)$$

由于 $A(f_{10}'' - f_0'' f_{10})$ 为小量, 且由式(3.6), 有 $f_{10}'(5.83) = 0$; 由式(3.4)及(3.8), 有 $f_0''(5.83) \times f_{10}(5.83) \approx 0$, 故 $f_{10}'' \approx f_0'' f_{10}$ 。因而 f_{10}'' 及 $f_0'' f_{10}$ 均为小量, 求近似解时, 我们假设 $f_{10}'' = 0$, 并按照式(4.7), 用 $f_0'' f_0$ 代换 $f_{10}'' f_{10}$, 即式(4.1)进一步简化成为

$$-\frac{1}{2}f_0 f_0'' + f_0'^2 - 1 - f_1'' - A f_0 f_0'' = 0 \quad (4.8)$$

边界条件仍然是式(3.6)。

将式(2.7), (2.8), (3.2)及(3.3)代入上式得

$$\begin{aligned} f_1'' &= \frac{3}{5} \left(\frac{\eta}{5.83} \right)^8 - \frac{12}{5} \left(\frac{\eta}{5.83} \right)^7 + \frac{5}{2} \left(\frac{\eta}{5.83} \right)^6 + \frac{9}{5} \left(\frac{\eta}{5.83} \right)^5 - \frac{9}{2} \left(\frac{\eta}{5.83} \right)^4 \\ &+ 3 \left(\frac{\eta}{5.83} \right)^2 - 1 - A \left(\frac{1}{5.83} \eta^2 - \frac{1}{5.83^3 \times 2} \eta^4 + \frac{1}{5.83^4 \times 5} \eta^5 \right) \\ &\cdot \left(\frac{2}{5.83} - \frac{6}{5.83^3} \eta^2 + \frac{4}{5.83^4} \eta^3 \right) = \frac{3}{5} \left(\frac{\eta}{5.83} \right)^8 - \frac{12}{5} \left(\frac{\eta}{5.83} \right)^7 \end{aligned}$$

$$\begin{aligned}
& + \frac{5}{2} \left(\frac{\eta}{5.83} \right)^6 + \frac{9}{5} \left(\frac{\eta}{5.83} \right)^5 - \frac{9}{2} \left(\frac{\eta}{5.83} \right)^4 + 3 \left(\frac{\eta}{5.83} \right)^2 - 1 \\
& + A \left[-\frac{4}{5} \left(\frac{\eta}{5.83} \right)^8 + \frac{16}{5} \left(\frac{\eta}{5.83} \right)^7 - 3 \left(\frac{\eta}{5.83} \right)^6 - \frac{22}{5} \left(\frac{\eta}{5.83} \right)^5 \right. \\
& \left. + 7 \left(\frac{\eta}{5.83} \right)^4 - 2 \left(\frac{\eta}{5.83} \right)^2 \right] \quad (4.9)
\end{aligned}$$

积分, 并利用式(3.4)得

$$\begin{aligned}
f_1'' &= 5.83 \left[\frac{1}{15} \left(\frac{\eta}{5.83} \right)^9 - \frac{3}{10} \left(\frac{\eta}{5.83} \right)^8 + \frac{5}{14} \left(\frac{\eta}{5.83} \right)^7 + \frac{3}{10} \left(\frac{\eta}{5.83} \right)^6 \right. \\
& - \frac{9}{10} \left(\frac{\eta}{5.83} \right)^5 + \left. \left(\frac{\eta}{5.83} \right)^3 - \frac{\eta}{5.83} \right] + A \left[-\frac{4}{45} \left(\frac{\eta}{5.83} \right)^9 \right. \\
& + \frac{2}{5} \left(\frac{\eta}{5.83} \right)^8 - \frac{3}{7} \left(\frac{\eta}{5.83} \right)^7 - \frac{11}{15} \left(\frac{\eta}{5.83} \right)^6 \\
& \left. + \frac{7}{5} \left(\frac{\eta}{5.83} \right)^5 - \frac{2}{3} \left(\frac{\eta}{5.83} \right)^3 \right] \cdot 5.83 + C_1' \quad (4.10)
\end{aligned}$$

再积分, 并利用 $f_1'(0) = 0$ 及式(3.5)得

$$\begin{aligned}
f_1' &= 5.83^2 \left[\frac{1}{150} \left(\frac{\eta}{5.83} \right)^{10} - \frac{1}{30} \left(\frac{\eta}{5.83} \right)^9 + \frac{5}{112} \left(\frac{\eta}{5.83} \right)^8 + \frac{3}{70} \left(\frac{\eta}{5.83} \right)^7 \right. \\
& - \frac{3}{20} \left(\frac{\eta}{5.83} \right)^6 + \frac{1}{4} \left(\frac{\eta}{5.83} \right)^4 - \left. \frac{1}{2} \left(\frac{\eta}{5.83} \right)^2 \right] \\
& + A \times 5.83^2 \left[-\frac{2}{225} \left(\frac{\eta}{5.83} \right)^{10} + \frac{2}{45} \left(\frac{\eta}{5.83} \right)^9 - \frac{3}{56} \left(\frac{\eta}{5.83} \right)^8 \right. \\
& - \frac{11}{105} \left(\frac{\eta}{5.83} \right)^7 + \frac{7}{30} \left(\frac{\eta}{5.83} \right)^6 - \left. \frac{1}{6} \left(\frac{\eta}{5.83} \right)^4 \right] + C_1' \eta \quad (4.11)
\end{aligned}$$

由 $f_1'(5.83) = 0$ 得

$$\begin{aligned}
C_1' \times 5.83 &= 1.9773 \times 5.83 - A \times 5.83^2 \left(-\frac{2}{225} + \frac{2}{45} \right. \\
& \left. - \frac{3}{56} - \frac{11}{105} + \frac{7}{30} - \frac{1}{6} \right)
\end{aligned}$$

由式(4.10)得

$$f_1''(0) = C_1' = 1.9773 + 0.3271A \quad (4.12)$$

由上式及式(3.14)得

$$\varphi'' = f_1''(0) + \xi f_1''(0) = 0.3431 + \xi(1.9773 + 0.3271A) \quad (4.13)$$

当 $A = 0$ 时, 上式变为式(3.16).

例2 设 $U = x - x^3$, 则 $\xi = 1 - 2x^2/(1 - x^2)$, $\zeta = -(\xi^2 - 4\xi + 3)$, $\therefore A = -3$. 由式(4.13)得

$$\varphi = 0.3431 + 0.9960\xi \quad (4.14)$$

图2表示一级近似下, 例2的流动的摩擦应力因子 φ 与纵坐标 x 的关系. 实曲线表示准确结果^[1], 虚线表示本文的一级近似结果, 即式(4.14). 由图2可见, 在 $x = 0 \sim 0.44$ 的范围

内, 本文的误差小于10%, 只是在分离点附近, 才有较大的误差。

当 $\varphi=0$ 时, 流动发生分离, 由式(4.14)得

$$\xi = -0.3431/0.996 = -0.3445,$$

$$x = \sqrt{(1-\xi)/(3-\xi)} = 0.634. \text{ 准确值为}^{[1]}$$

$$x = 0.66, \text{ 误差为} 4\%.$$

将式(4.11)再积分一次, 并利用边界条件, $f_1(0)=0$, 便得

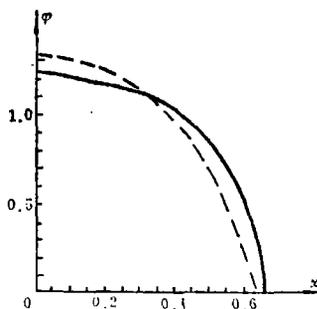


图 2

$$\begin{aligned} f_1(\eta) = & 5.83^3 \left[\frac{1}{1650} \left(\frac{\eta}{5.83} \right)^{11} - \frac{1}{300} \left(\frac{\eta}{5.83} \right)^{10} + \frac{5}{1008} \left(\frac{\eta}{5.83} \right)^9 \right. \\ & \left. + \frac{3}{560} \left(\frac{\eta}{5.83} \right)^8 - \frac{3}{140} \left(\frac{\eta}{5.83} \right)^7 + \frac{1}{20} \left(\frac{\eta}{5.83} \right)^6 - \frac{1}{6} \left(\frac{\eta}{5.83} \right)^5 \right] \\ & + A \times 5.83^3 \left[-\frac{2}{225 \times 11} \left(\frac{\eta}{5.83} \right)^{11} + \frac{1}{45 \times 5} \left(\frac{\eta}{5.83} \right)^{10} \right. \\ & \left. - \frac{1}{56 \times 3} \left(\frac{\eta}{5.83} \right)^9 - \frac{11}{105 \times 8} \left(\frac{\eta}{5.83} \right)^8 + \frac{1}{30} \left(\frac{\eta}{5.83} \right)^7 \right. \\ & \left. - \frac{1}{30} \left(\frac{\eta}{5.83} \right)^5 \right] + C_1 \eta^2 / 2 \end{aligned}$$

故

$$\begin{aligned} f_1(\eta) = & 198.16 \left[\left(\frac{1}{1650} - \frac{2A}{2475} \right) \left(\frac{\eta}{5.83} \right)^{11} + \left(-\frac{1}{300} \right. \right. \\ & \left. \left. + \frac{A}{225} \right) \left(\frac{\eta}{5.83} \right)^{10} + \left(\frac{5}{1008} - \frac{A}{168} \right) \left(\frac{\eta}{5.83} \right)^9 + \left(\frac{3}{560} - \frac{11}{840} \right. \right. \\ & \left. \left. \times A \right) \left(\frac{\eta}{5.83} \right)^8 + \left(-\frac{3}{140} + \frac{A}{30} \right) \left(\frac{\eta}{5.83} \right)^7 + \left(\frac{1}{20} - \frac{A}{30} \right) \left(\frac{\eta}{5.83} \right)^5 \right. \\ & \left. - \frac{1}{6} \times \left(\frac{\eta}{5.83} \right)^3 \right] + (0.9887 + 0.1636A) \eta^2 \end{aligned} \quad (4.15)$$

$$f = f_0 + \xi f_1 \quad (4.16)$$

于是, 式(4.15), (4.16)及(2.7)便构成了层流边界层方程的一级近似分析解。

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An Approximate Analytical Solution of the Laminar Boundary Layer Equations

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Abstract

Using the pressure gradient as the new variable instead of the ordinary longitudinal coordinate x , Liu transformed the ordinary laminar boundary equations into a new form. On this base Liu obtained the frictional stress factor by using the graphical method.

In this paper the same variable replacement as in [1] is used and an approximate analytical solution of the laminar boundary layer equations by the series method is obtained. The author also obtains a formula of frictional stress factor. For the case of the main function without the term of constant the author makes a further simplification. The error of the frictional stress factor obtained by the author is still less than 10% compared with that of [1].

Key words laminar boundary layer, pressure gradient, frictional stress factor