

弹性薄板的样条梁函数解法*

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摘 要

本文从三次及二次样条梁函数定义的四阶及三阶的广义梁的微分方程出发, 由于采用了广义函数, 可推导出连续荷载、间断荷载、集中荷载、集中弯矩等各种荷载及各种边界条件(简支、固支、自由)下的多项式梁函数。用最小势能原理推导弹性薄板变形曲面及应力, 均获得精度较高的近似解。

一、梁函数的推导

弹性薄板经典解法^[1]采用了双曲线函数及三角级数解法, 在集中荷载、集中弯矩作用下收敛缓慢。本文推导的梁函数适应广泛条件, 尤其是采用多项式克服收敛慢的缺点, 获得精度较高的近似解。

本文采用三次样条函数定义的四阶广义梁的微分方程^[3]

$$\frac{d^4 w}{dx^4} = \sum_i P_i \delta(x-x_i) \quad (1.1)$$

狄拉克函数 δ 定义如下:

设 q 为匀布荷载, $q = \delta(x-\varepsilon)$ 相当于在 $x = \varepsilon$ 处有一个单位集中荷载, $\delta(x-\varepsilon)$ 的数学定义简单地说是: 在 $x \neq \varepsilon$ 处, $\delta(x-\varepsilon) = 0$; 在 $x = \varepsilon$ 处, $\delta(x-\varepsilon) = \infty$

并且
$$\int_0^l \delta(x-\varepsilon) dx = 1$$

因此如果某一个函数 $f(x)$ 在 $x = \varepsilon$ 是连续的, 则有:

$$\int_0^l f(x) \delta(x-\varepsilon) dx = \int_0^l f(\varepsilon) \delta(x-\varepsilon) dx = f(\varepsilon) \int_0^l \delta(x-\varepsilon) dx = f(\varepsilon)$$

公式(1.1)的解可写为:

$$w = c_0 + c_1 x + c_2 \frac{x^2}{2!} + c_3 \frac{x^3}{3!} + \sum_{i=1}^{N-1} \frac{P_i (x-x_i)_+^3}{3!} \quad (1.2)$$

$$\frac{d^3 w}{dx^3} = \sum_i M_i \delta(x-x_i) \quad (\text{二次样条函数定义微分方程}) \quad (1.3)$$

* 钱伟长推荐。

的解:
$$w = c_0 + c_1 x + \frac{c_2}{2} x^2 + \sum_{i=1}^{N-1} \frac{M_i (x-x_i)_+^2}{2!} \quad (1.4)$$

在任意边界条件及任意荷载作用下, 都可求得梁函数 x 多项式的精确解:

1. 三次样条函数的推导

$$\frac{d^4 w}{dx^4} = \sum_i P_i \delta(x-x_i) \quad (1.5)$$

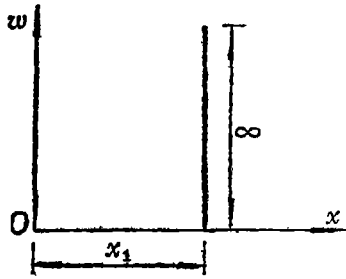


图 1

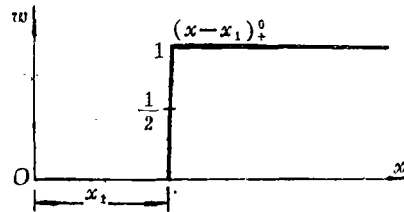


图 2

为简单计, 图形均绘出 x_i 一个 ($i=1$), x_i 如有多个, 则应有多个间断的图形, 积分一次可得:

$$\frac{d^3 w}{dx^3} = c_3 + \sum_i P_i (x-x_i)_+^{0 \ 1)} \quad (1.6)$$

如图 2 所示.

积分二次 (图 3)

$$\frac{d^2 w}{dx^2} = c_2 + c_3 x + \sum_{i=1}^{N-1} P_i (x-x_i)_+^{2 \ 2)} \quad (1.7)$$

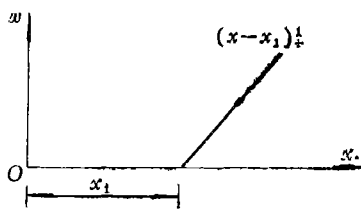


图 3

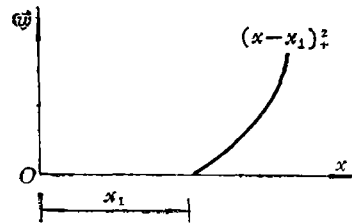


图 4

积分三次 (图 4)

$$\frac{dw}{dx} = c_1 + c_2 x + c_3 \frac{x^2}{2!} + \sum_{i=1}^{N-1} \frac{P_i (x-x_i)_+^2}{2!} \quad (1.8)$$

积分四次 (图 5)

$$w = c_0 + c_1 x + c_2 \frac{x^2}{2!} + c_3 \frac{x^3}{3!} + \sum_{i=1}^{N-1} \frac{P_i (x-x_i)_+^3}{3!} \quad (1.9)$$

- 1) 可写成 $\delta(x-x_i)$ 函数, 即阶跃函数.
- 2) +为间断符号.

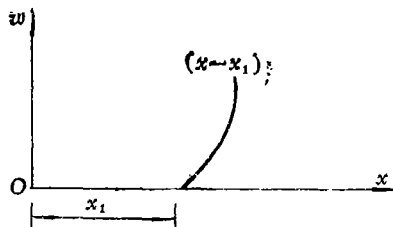


图 5

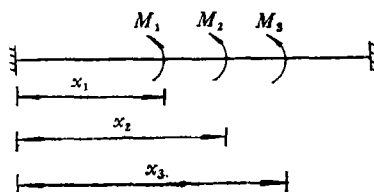


图 6

2. 二次样条函数为三阶导数的广义微分方程，可以表达集中弯矩，比较方便。

$$\frac{d^3 w}{dx^3} = \sum_{i=1}^{N-1} M_i \delta(x-x_i) \tag{1.10}$$

微分一次

$$\frac{d^4 w}{dx^4} = \sum_{i=1}^{N-1} M_i \delta'(x-x_i) \tag{1.11}$$

这仍然是广义梁微分方程，如果加集中荷载项可写成：

$$\frac{d^4 w}{dx^4} = \sum_{i=1}^{N-1} M_i \delta'(x-x_i) + \sum_{i=1}^{N-1} P_i \delta(x-x_i) \tag{1.12}$$

匀布荷载 q 写成：

$$\frac{d^4 w}{dx^4} = \frac{q}{EI} \tag{1.13}$$

即普通梁的微分方程，如果是部分间断匀布荷载：

$$EI = \frac{d^4 w}{dx^4} q [\delta(x-x_1) - \delta(x-x_2)]$$

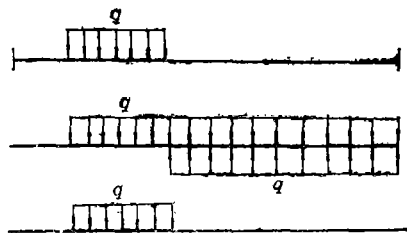


图 7

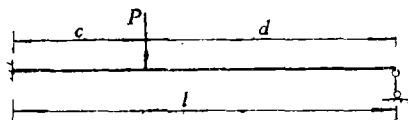


图 8

任意边界可用四个积分常数定出。

3. 变形曲线的推导

左端固定，右端铰支梁，梁上有一个集中荷载 P (图8)

$$w = c_0 + c_1 x + c_2 \frac{x^2}{2!} + c_3 \frac{x^3}{3!} + \frac{P(x-c)_+^3}{3!}$$

$$w' = c_1 + c_2 x + c_3 \frac{x^2}{2!} + \frac{P(x-c)^2_+}{2!}, \quad w'' = c_2 + c_3 x + P(x-c)_+$$

$$x=0 \text{ 时: } w=0, \quad c_0=0; \quad x=0 \text{ 时: } w'=0, \quad c_1=0;$$

$$x=l \text{ 时: } w=0, \quad c_2 \frac{l^2}{2} + c_3 \frac{l^3}{6} + \frac{Pd^3}{6} = 0$$

$$x=l \text{ 时: } w''=0, \quad c_2 + c_3 l + Pd = 0$$

$$\text{联解} \quad c_2 = \frac{Pd}{2} \left(1 - \frac{d^2}{l^2}\right), \quad c_3 = -\frac{3Pd}{2l} \left(1 - \frac{d^2}{3l^2}\right)$$

变形曲线 (分成两部份)

$$\left. \begin{aligned} w &= \frac{Pd}{4} x^2 \left(1 - \frac{d^2}{l^2}\right) - \frac{1}{4} \frac{Pd}{l} x^3 \left(1 - \frac{d^2}{3l^2}\right) \quad (0 \leq x \leq c) \\ w &= \frac{Pd}{4} x^2 \left(1 - \frac{d^2}{l^2}\right) - \frac{1}{4} \frac{Pd}{l} x^3 \left(1 - \frac{d^2}{3l^2}\right) + \frac{P(x-c)^3}{6} \quad (c \leq x \leq l) \end{aligned} \right\} \quad (1.14)$$

与材料力学结果相同, 其它边界条件和各种荷载都可相似推出. 以下列出几种梁函数:

两端简支梁承受匀布荷载 q 挠度曲线为 (图9):

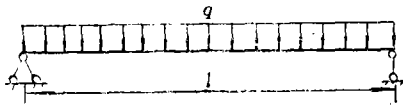


图 9

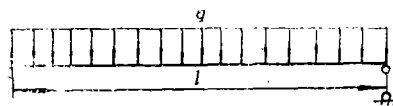


图 10

$$w = \frac{ql^4}{24EI} \left(\frac{x^4}{l^4} - 2 \frac{x^3}{l^3} + \frac{x}{l} \right) \quad (1.15)$$

左端固支, 右端简支受有匀布荷载 q 为 (图10):

$$w = \frac{ql^4}{48EI} \left(2 \frac{x^4}{l^4} - 5 \frac{x^3}{l^3} + 3 \frac{x^2}{l^2} \right) \quad (1.16)$$

两端固支梁受有匀布荷载 q 挠度曲线为 (图11):

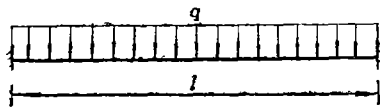


图 11

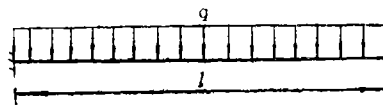


图 12

$$w = \frac{ql^4}{24EI} \left(\frac{x^4}{l^4} - 2 \frac{x^3}{l^3} + \frac{x^2}{l^2} \right) \quad (1.17)$$

两端简支梁, 中点作用集中荷载 P 挠度曲线为:

$$0 \leq x \leq \frac{l}{2}, \quad w = \frac{P}{48EI} \left(3 \frac{x}{l} - 4 \frac{x^3}{l^3} \right) \quad (1.18)$$

左端固支, 右端自由悬臂梁承受匀布荷载 q 为 (图12):

$$w = \frac{ql^4}{24EI} \left(\frac{x^4}{l^4} - 4 \frac{x^3}{l^3} + 6 \frac{x^2}{l^2} \right) \quad (1.19)$$

二、样条函数在矩形薄板解法中的应用

在等厚度各向同性板形变势能为:

$$U = \frac{D}{2} \iint \left\{ (\nabla^2 w)^2 - 2(1-\mu) \left[\frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} - \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] \right\} dx dy \quad (2.1)$$

式(2.1)中第二个积分可以变换成为:

$$\begin{aligned} \iint \left[\frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} - \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] dx dy &= \iint \left[\frac{\partial}{\partial x} \left(\frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial y^2} \right) \right. \\ &\quad \left. - \frac{\partial}{\partial y} \left(\frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial x \partial y} \right) \right] dx dy \end{aligned} \quad (2.2)$$

根据格林定理

$$\iint \left[\frac{\partial}{\partial x} P(x, y) - \frac{\partial}{\partial y} Q(x, y) \right] dx dy = \int [Q(x, y) dx + P(x, y) dy] \quad (2.3)$$

于是可由上式得:

$$\iint \left[\frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} - \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] dx dy = \oint \left[\frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial x \partial y} dx + \frac{\partial w}{\partial x} \frac{\partial^2 w}{\partial y^2} dy \right] \quad (2.4)$$

其中右边线积分是沿薄板边界进行的。

$$\frac{\partial}{\partial x} = \frac{\partial}{\partial n}, \quad \frac{\partial}{\partial y} = \frac{\partial}{\partial l} \quad (2.5)$$

n, l 为外法线方向, 对于具有平行于轴 Ox 和 Oy 的边界的矩形板, 在平行于轴 Oy 的边上, 公式成立(图13)。

因此, 如果平行于轴 Oy 的边是简支边, 那末有

$$w=0, \quad M_x = -D \left(\frac{\partial^2 w}{\partial x^2} + \mu \frac{\partial^2 w}{\partial y^2} \right) = 0$$

$$\text{边界是刚性边, 因此有 } w=0, \quad \frac{\partial^2 w}{\partial x^2} = 0 \quad (2.6)$$

$$\text{如果是刚性固定, 那末有 } w=0, \quad \frac{\partial w}{\partial x} = 0 \quad (2.7)$$

如果平行于 Oy 轴的边是自由的, 那末有:

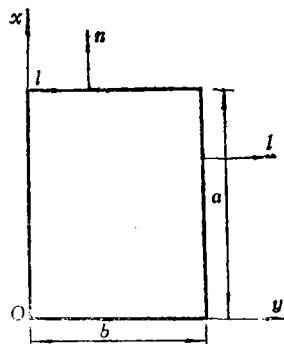


图 13

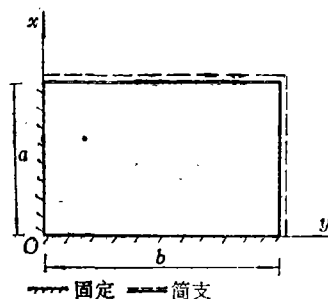


图 14

$$\frac{\partial^2 w}{\partial x^2} + \mu \frac{\partial^2 w}{\partial y^2} = 0, \quad \frac{\partial^3 w}{\partial x^3} + (2-\mu) \frac{\partial^3 w}{\partial x \partial y^2} = 0 \quad (2.8)$$

如果一个矩形薄板没有自由边, 而只有固定和简支边, 则形变势能简化为:

$$U = \frac{D}{2} \iint (\nabla^2 w)^2 dx dy \quad (2.9)$$

算例 1 两邻边固定, 两邻边简支 (图14), 弹性薄板承受匀布荷载 q , 求中点挠度. 板的挠度可写成为:

$$w = CXY = \left(2 \frac{x^4}{a^4} - 5 \frac{x^3}{a^3} + 3 \frac{x^2}{a^2}\right) \left(2 \frac{y^4}{b^4} - 5 \frac{y^3}{b^3} + 3 \frac{y^2}{b^2}\right) (c_1 + c_2 x^2 + c_3 y^2 + c_4 xy + \dots) \quad (2.10)$$

取 X, Y 都为梁函数, 用一端固定, 一端简支公式(1.16), 由于用最小势能原理计算薄板, 梁函数常数因子 $q/48EI$ 乘积无关所设. 待定系数 c_1, c_2, \dots, c_r 可取 r 项, 由于梁函数精确满足边界条件, 一般只取一项.

泛函数可写成

$$\begin{aligned} \Pi &= \frac{D}{2} \int_0^a \int_0^b (\nabla^2 w)^2 dx dy - q \int_0^a \int_0^b w dx dy \\ &= \frac{D}{2} \left[\int_0^a X''^2 dx \int_0^b Y^2 dy + 2 \int_0^a X X'' dx \int_0^b Y Y'' dy \right. \\ &\quad \left. + \int_0^a X^2 dx \int_0^b Y''^2 dy \right] c_1^2 - q c_1 \int_0^a X dx \int_0^b Y dy \end{aligned} \quad (2.11)$$

$$\int_0^a X^2 dx = \int_0^a \left(2 \frac{x^4}{a^4} - 5 \frac{x^3}{a^3} + 3 \frac{x^2}{a^2}\right)^2 dx = 0.03015a$$

$$\int_0^a X''^2 dx = \int_0^a \left[6 \left(4 \frac{x^2}{a^2} - 5 \frac{x}{a} + 1\right) \frac{1}{a^2}\right]^2 dx = 7.2 \frac{1}{a^3}$$

$$\int_0^a X X'' dx = \int_0^a 6 \left(4 \frac{x^2}{a^2} - 5 \frac{x}{a} + \frac{1}{a^2}\right) \left(2 \frac{x^4}{a^4} - 5 \frac{x^3}{a^3} + 3 \frac{x^2}{a^2}\right) dx = -0.342857 \frac{1}{a}$$

$$\int_0^a X dx = \int_0^a \left(2 \frac{x^4}{a^4} - 5 \frac{x^3}{a^3} + 3 \frac{x^2}{a^2}\right) dx = 0.15a$$

于是梁函数解算弹性薄板, 归结为以上四种类型积分. 梁函数 Y 的四种类型积分比例同一种梁函数, 因此只须相应代换 Y 换 X , y 换 x , b 换 a 即可. 根据最小势能原理, $\delta \Pi = 0$

$$c_1 = \frac{0.15 \times 0.15ab}{7.2 \times 0.03015 \left(\frac{b}{a^3} + \frac{a}{b^3}\right) + 2 \frac{1}{ab} (-0.342857)^2} \frac{q}{D}$$

求方板中点挠度以便与经典解相对照 ($a=b$).

$$c_1 = \frac{0.15 \times 0.15}{7.2 \times 0.03015 \times 2 + 2(-0.342857)^2} \frac{qa^4}{D} = 0.0336216 \frac{qa^4}{D}$$

以 $x=a/2, y=b/2$ 代入挠度表达式(2.10)得:

$$w_0 = 0.0336216 \frac{qa^4}{D} \times \frac{1}{4} \times \frac{1}{4} = 0.00210135 \frac{qa^4}{D}$$

与经典解对照, 误差极微。

算例 2 一边固定, 三边简支矩形薄板承受匀布荷载 q , 求板中心挠度(图15)。

取挠度曲线为:

$$w=CXY=c_1\left(\frac{x^4}{a^4}-2\frac{x^3}{a^3}+\frac{x}{a}\right)\left(2\frac{y^4}{b^4}-5\frac{y^3}{b^3}+3\frac{y^2}{b^2}\right) \quad (2.12)$$

梁函数 X, Y 用(1.15), (1.16)式。

$$\int_0^a X^2 dx = 0.0492056a, \quad \int_0^b Y^2 dy = 0.03015b$$

$$\int_0^a X''^2 dx = 4.799952 \frac{1}{a^3}, \quad \int_0^b Y''^2 dy = 7.2 \frac{1}{b^3}$$

$$\int_0^a X'' X dx = -0.485676 \frac{1}{a}, \quad \int_0^b Y'' Y dy = -0.342857 \frac{1}{b}$$

$$\int_0^a X dx = 0.2a, \quad \int_0^b Y dy = 0.15b$$

由 $\delta\Pi=0$ 可得:

$$c_1 = \frac{0.2a \times 0.15b}{4.8 \frac{1}{a^3} \times 0.03015b + 2 \frac{(-0.485676) \times (-0.342857)}{ab} + 0.0492056a \times 7.2 \frac{1}{b^3}} \frac{q}{D}$$

$$= \frac{0.03ab}{0.144718 \frac{b}{a^3} + 0.333035 \frac{1}{ab} + 0.354280 \frac{a}{b^3}} \frac{q}{D}$$

方板 $a=b$, $c_1 = \frac{0.03a^2}{0.832033 \frac{1}{a^2}} \frac{q}{D} = 0.0360562 \frac{qa^4}{D}$

代入挠度表达式(2.12), 令 $x=a/2, y=a/2, a=b$

$$w_c = 0.0360562 \frac{qa^4}{D} \times 0.3125 \times \frac{1}{4} = 0.0028169 \frac{qa^4}{D}$$

与经典解^[1] $0.00280qa^4/D$ 比较, 误差不及百分之一。

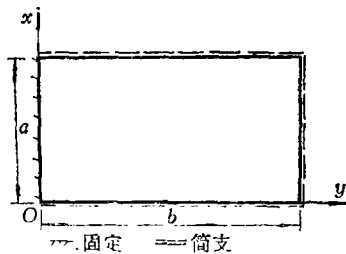


图 15

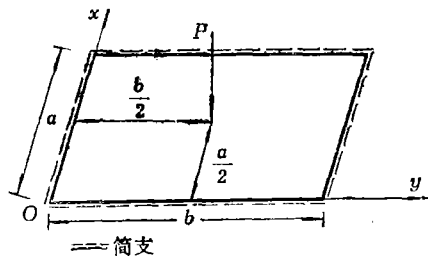


图 16

算例 3 四边简支薄板, 中点有集中荷载 P , 设 $\mu=0.3$ 求中点挠度(图16)。

挠度表达式为:

$$w=CXY=c_1\left(3\frac{x}{a}-4\frac{x^3}{a^3}\right)\left(3\frac{y}{b}-4\frac{y^3}{b^3}\right) \quad \left(0 \leq x \leq \frac{a}{2}\right) \quad (2.13)$$

梁函数 X, Y 都用公式(1.18),

$$\left. \begin{aligned} \int_0^{\frac{a}{2}} X^2 dx &= 0.2428571a, & \int_0^{\frac{a}{2}} X'' X dx &= -2.4 \frac{1}{a} \\ \int_0^{\frac{a}{2}} X''^2 dx &= 24 \frac{1}{a^3}, & X_{x=a/2} &= Y_{y=b/2} = 1 \end{aligned} \right\} \quad (2.14)$$

泛函可写成 $\Pi = \frac{D}{2} \int_0^a \int_0^b (\nabla^2 w)^2 dx dy - Pw_{(x=a/2, y=b/2)}$ 集中荷载 P 所做的功, w 取 $x=a/2, y=b/2$ 点的挠度. 由于荷载作用在中点泛函又可写成:

$$\begin{aligned} \Pi &= \frac{4D}{2} \int_0^{\frac{a}{2}} \int_0^{\frac{b}{2}} (\nabla^2 w)^2 dx dy - Pw_{(x=a/2, y=b/2)} \\ &= \frac{4D}{2} \left[\int_0^{\frac{a}{2}} X''^2 dx \int_0^{\frac{b}{2}} Y^2 dy + 2 \int_0^{\frac{a}{2}} X X'' dx \int_0^{\frac{b}{2}} Y Y'' dy \right. \\ &\quad \left. + \int_0^{\frac{a}{2}} X^2 dx \int_0^{\frac{b}{2}} Y''^2 dy \right] c_1^2 - c_1 Pw_{(x=a/2, y=b/2)} \end{aligned} \quad (2.15)$$

(2.14)代入(2.15), $\partial \Pi / \partial c_1 = 0$, 注意梁函数 X, Y 相同, 符号互换

$$c_1 = \frac{1 \times 1}{4 \left[0.2428571 \times 24 \times \left(\frac{b}{a^3} + \frac{a}{b^3} \right) + 2 \times (-2.4)^2 \frac{1}{ab} \right]} \frac{P}{D}$$

方板中点挠度($a=b, x=a/2, y=b/2$):

$$c_1 = \frac{1 \times 1}{4 \times (11.65714 + 11.52)} \frac{1}{a^2} \frac{P}{D} = 0.0107864 \frac{Pa^2}{D}$$

代回挠度表达式(2.13)

$$w_0 = 0.0107864 \frac{Pa^2}{D} \times 1 \times 1 = 0.0107864 \frac{Pa^2}{D}$$

经典解集中荷载级数取很多项, 甚至十几项, 用样条函数推导的梁函数, 只须取一项或二项达到很高精度, 这是本法突出优点.

算例 4 两对边简支, 一边固定, 一边自由的弹性薄板承受匀布荷载 q 如图 17 所示, 设 $\mu=0.3$ 求矩形板中点挠度.

有自由边的弹性薄板泛函可写成为:

$$\begin{aligned} \Pi &= \frac{D}{2} \iint \left\{ (\nabla^2 w)^2 - 2(1-\mu) \left[\frac{\partial^2 w}{\partial x^2} \frac{\partial^2 w}{\partial y^2} - \left(\frac{\partial^2 w}{\partial x \partial y} \right)^2 \right] \right\} dx dy - q \iint w dx dy \\ &= \frac{D}{2} \left\{ \left[\int_0^a X''^2 dx \int_0^b Y^2 dy + 2 \int_0^a X'' X dx \int_0^b Y'' Y dy + \int_0^a X^2 dx \int_0^b Y''^2 dy \right] \right. \\ &\quad \left. - 2(1-\mu) \left[\int_0^a X'' X dx \int_0^b Y'' Y dy - \int_0^a X'^2 dx \int_0^b Y'^2 dy \right] \right\} c_1^2 - qc_1 \int_0^a X dx \int_0^b Y dy \end{aligned}$$

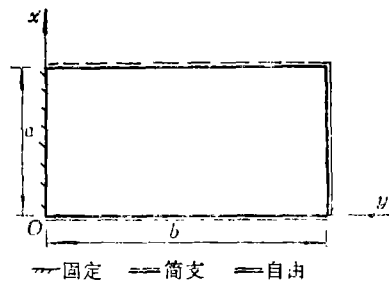


图 17

$$\text{挠度表达式为: } w = CXY = c_1 \left(\frac{x^4}{a^4} - 2\frac{x^3}{a^3} + \frac{x}{a} \right) \left(\frac{y^4}{b^4} - 4\frac{y^3}{b^3} + 6\frac{y^2}{b^2} \right) \quad (2.16)$$

X, Y 梁函数取自公式(1.15), (1.19),

$$\begin{aligned} \int_0^a X^2 dx &= 0.049206a, & \int_0^b Y^2 dy &= 2.311111b \\ \int_0^a X''^2 dx &= 4.799952 \frac{1}{a^3}, & \int_0^b Y''^2 dy &= 28.8 \frac{1}{b^3} \\ \int_0^a X'' X dx &= -0.485676 \frac{1}{a}, & \int_0^b Y'' Y dy &= 1.714286 \frac{1}{b} \\ \int_0^a X'^2 dx &= -0.485714 \frac{1}{a}, & \int_0^b Y'^2 dy &= 10.285714 \frac{1}{b} \\ \int_0^a X dx &= 0.2a, & \int_0^b Y dy &= 1.2b \end{aligned}$$

X, Y 函数不同, 各有五种类型积分.

$$\Pi = -\frac{D}{2} \{ [4.799952 \times 2.311111 + 2 \times 1.714286 \times (-0.485676)] + 28.8 \times 0.049206 \}$$

$$- 2(1-0.3)[-0.485676 \times 1.714286 - 0.485714 \times 10.285714] \} c_1^2 - c_1 q \times 0.2 \times 1.2$$

由 $\delta\Pi = 0$, 求方板自由边中点挠度 ($a=b$),

$$c_1 = \frac{0.2 \times 1.2 a^2}{19.005072 \frac{1}{a^2}} \frac{q}{D} = 0.0126282 \frac{qa^4}{D}$$

方板自由边中点的挠度

$$w_{f,c} = 0.0126282 \frac{qa^4}{D} \times 0.3125 \times 3 = 0.011839 \frac{qa^4}{D}$$

与经典解比较, 误差不及 2%.

算例 5 二对边简支, 一边固定一边自由矩形板 (图 18). 在自由边中点作用集中荷载 P , $\mu=0.3$, 求方板中点挠度及自由边中点挠度.

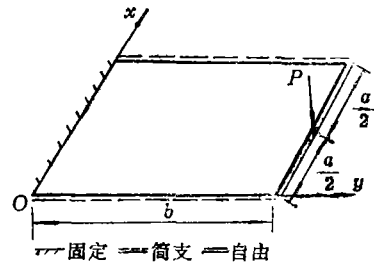


图 18

$$\begin{aligned} \Pi = & \frac{\lambda 2D}{2} \left\{ \int_0^{\frac{a}{2}} X''^2 dx \int_0^b Y^2 dy + 2\mu \int_0^{\frac{a}{2}} X'' X dx \int_0^b Y'' Y dy + \int_0^{\frac{a}{2}} X^2 dx \int_0^b Y''^2 dy \right. \\ & \left. + 2(1-\mu) \int_0^{\frac{a}{2}} X'^2 dx \int_0^b Y'^2 dy \right\} c_1^2 - P c_1 \times 1 \times 2 \end{aligned} \quad (2.17)$$

$$\text{梁函数为: } X = \left(3\frac{x}{a} - 4\frac{x^3}{a^3} \right), \quad Y = \left(3\frac{y^2}{b^2} - \frac{y^3}{b^3} \right)$$

$$\int_0^{\frac{a}{2}} X dx = 0.2428571a, \quad \int_0^b Y^2 dy = \frac{33}{35} b$$

$$\int_0^{\frac{a}{2}} X''^2 dx = 24 \frac{1}{a^3}, \quad \int_0^b Y''^2 dy = 12 \frac{1}{b^3}$$

$$\int_0^{\frac{a}{2}} X'' X dx = -2.4 \frac{1}{a}, \quad \int_0^b Y'' Y dy = \frac{6}{5} \frac{1}{b}$$

$$\int_0^{\frac{a}{2}} X'^2 dx = 2.4 \frac{1}{a}, \quad \int_0^b Y'^2 dy = \frac{24}{5} \frac{1}{b}$$

$$X_{x=a/2} = 1, \quad Y_{y=b} = 2$$

极值条件 $\partial \Pi / \partial c_1 = 0$

$$2c_1 \left[24 \frac{1}{a^3} \times \frac{33}{35} b + 0.3 \left(-2.4 \frac{1}{a} \right) \left(\frac{6}{5} \frac{1}{b} \right) + 0.24286a \times 12 \frac{1}{b^3} \right. \\ \left. + 1.4 \times 2.4 \frac{1}{a} \times \frac{24}{5} \frac{1}{b} \right] = \frac{P}{D} \times 1 \times 2$$

方板 ($a=b$): $c_1 = 0.025036 \frac{Pa^2}{D}$

方板中点的挠度为:

$$w_0 = 0.025036 \frac{Pa^2}{D} \times 1 \times \frac{5}{8} = 0.0156475 \frac{Pa^2}{D}$$

自由边中点挠度为:

$$w_{f,c} = 0.025036 \frac{Pa^2}{D} \times 1 \times 2 = 0.050072 \frac{Pa^2}{D}$$

从本文算例可以看出, 在任意荷载、任意边界条件情况下, 用一级近似可求得板中点挠度较好的近似解。

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Solution of Spline Function of Elastic Plates

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Abstract

In this paper, from four- and three-order differential equations defined by cubic and quadratic splines of generalized beam. The beam functions with many boundary conditions and under various loads are reduced. The approximate solution of deformation surface and stress of elastic thin plate is very accurate.