

# 润滑理论中的广义雷诺方程 和不等变分问题\*

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## 摘 要

本文运用张量分析工具和S-坐标系, 推导了润滑理论中的广义雷诺方程及相应的不等变分问题, 它计及了润滑流动中的弯曲效应, 轴和轴瓦曲面内蕴性质对流动的影响。

## 一、前 言

润滑理论是以雷诺方程为研究的出发点, 雷诺方程是在略去惯性项, 并假定轴和轴瓦曲面 $S_b$ ,  $S_a$ 的曲率半径为无限大时, 线性化Navier-Stokes方程而得到的, 因而它忽略了曲线运动产生的弯曲效应. 1950年G. H. Wannier<sup>[2]</sup>及1960年H. G. Elrod<sup>[3]</sup>, 分别用小参数方法, 在一级近似里, 导出了圆柱坐标系中的不可压的广义雷诺方程:

$$\frac{\partial}{\partial x} \left\{ h^3 \left( 1 - \frac{h}{D} \right) \frac{\partial p}{\partial x} \right\} + \frac{\partial}{\partial z} \left\{ h^3 \left( 1 + \frac{h}{D} \right) \frac{\partial p}{\partial z} \right\} = 6\mu U \frac{\partial}{\partial x} \left\{ h \left( 1 - \frac{h}{3D} \right) \right\} \quad (1.1)$$

其中 $D$ 为轴径,  $x$ 是旋转方向之弧长. 而G. Capriz<sup>[1]</sup>导出了在正交曲线坐标系中不可压之广义雷诺方程.

$$\begin{aligned} & \frac{\partial}{\partial x^1} \left\{ \frac{h^3}{\mu} \sqrt{\frac{a_2}{a_1}} \frac{\partial p}{\partial x^1} \right\} + \frac{\partial}{\partial x^2} \left\{ \frac{h^3}{\mu} \sqrt{\frac{a_1}{a_2}} \frac{\partial p}{\partial x^2} \right\} \\ & = 12\sqrt{a_1 a_2} V_3 + 6h^2 \frac{\partial}{\partial x^1} \left( \frac{\sqrt{a_2} V_1}{h} \right) + 6h^2 \frac{\partial}{\partial x^2} \left\{ \frac{\sqrt{a_1} V_2}{h} \right\} \end{aligned} \quad (1.2)$$

其中 $S_a$ 之度量张量是  $a_{11}=a_1$ ,  $a_{12}=a_{21}=0$ ,  $a_{22}=a_2$ .

本文采用 $S_a$ —坐标系, 运用张量分析工具, 导出了可压和不可压之广义雷诺方程

$$\begin{aligned} & \frac{\partial}{\partial x^\alpha} \left( \frac{\rho \sqrt{a}}{12\mu} h^3 B_\beta^\alpha a^{\beta\sigma} \frac{\partial p}{\partial x^\sigma} \right) = \frac{\partial}{\partial x^\alpha} \left( \frac{\rho^2 h^3 \sqrt{a}}{12\mu} B_\beta^\alpha X^\beta \right) \\ & + \frac{\partial}{\partial x^\alpha} \left( \frac{1}{2} \rho \sqrt{a} h B_\beta^\alpha (V_\beta^\beta - U^\beta) \right) + \sqrt{a} \frac{\partial}{\partial t} (h\rho) + \sqrt{a} \rho (V_\beta^\beta - U^\beta) \end{aligned} \quad (1.3)$$

其中 $B_\beta^\alpha$ 是由(3.20)所确定的二阶混合张量,  $a_{\alpha\beta}$ ,  $b_{\alpha\beta}$ 分别为曲面 $S_a$ 之第一、第二基本型,  $a$ 为度量张量 $a_{\alpha\beta}$ 的行列式,  $\mu$ 为流体粘性系数.

\* 钱伟长推荐.

方程(1.3)直接包含了曲面  $S_a$ ,  $S_b$  之内蕴性质, 它不但在方程右端, 而且在方程主部内包含了第一、第二基本型, 平均曲率和全曲率, 直接反映了曲线运动性质, 体现了由于曲线运动所产生的弯曲效应.

方程(1.3)在某种约束条件和满足一定的边值条件下求解, 由于它对应于一个凸集上泛函的极小化问题, 因而是一个不等变分问题, 它可借助数学规划理论, 进行数值计算.

方程(1.3)对可压和不可压情形均适用.

## 二、 $S_g$ —坐标系

润滑流体在两个曲面  $S_a$ ,  $S_b$  之间, 经受曲线运动, 曲面  $S_a$ ,  $S_b$  在某一方面是封闭的, 它们之间也作相对运动,  $S_a$  与  $S_b$  所夹的空间是一个狭窄地带, 沿  $S_a$  之法线方向,  $S_a$ ,  $S_b$  之间距离  $h(x^\alpha)$  称为这一地带之厚度, 若  $L$  为  $S_a, S_b$  之特征长度, 那么  $\frac{h}{L} \ll 1$ .

曲面  $S$  作为基础曲面, 在上取其高斯坐标系  $(x^\alpha)$ , 空间任一点  $P$ , 它的矢径  $R$  可以表示为

$$R = r + x^3 n$$

其中  $r$  为  $S$  上  $M$  点之矢径,  $n$  为  $S$  过  $M$  点之单位法线向量,  $P$  在这一法线上任一点,  $x^3$  坐标线恰是  $S$  的法线.  $x^3 = \text{const}$  是  $S$  之“平行”曲面, 它和  $S$  有同样的法线方向.

以后无特别声明, 希腊字母  $\alpha, \beta, \gamma \dots$  跑过 1, 2, 而拉丁字母  $i, j, k, \dots$  跑过 1, 2, 3, 上下指标相同者, 表示求和.

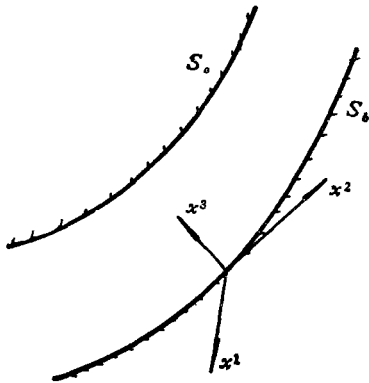


图1 局部标架.

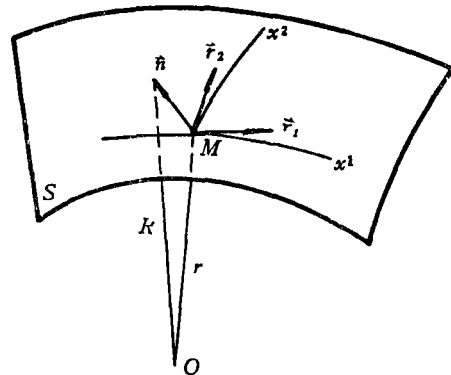


图2  $S_g$ —坐标系.

若取仿射标架之基矢量为

$$R_\alpha = r_\alpha + n_\alpha x^3, \quad R_3 = n \quad (2.1)$$

$r_\alpha$  是  $S$  上高斯坐标系之基矢量

$$\left. \begin{aligned} n_\alpha &= \frac{\partial n}{\partial x^\alpha} = -b_\alpha^i r_i \\ b_\alpha^i &= a^{\lambda\beta} b_{\beta\alpha} \\ a^{\alpha\beta} a_{\beta\gamma} &= \delta_\gamma^\alpha \end{aligned} \right\} \quad (2.2)$$

其中  $a_{\alpha\sigma}$ ,  $b_{\alpha\beta}$  为曲面  $S$  之第一、第二基本型。这样建立起来的坐标系, 称为  $S_0$ —坐标系。

在  $S_0$ —坐标系中, 三维欧氏空间之度量张量  $g_{ij} = \mathbf{R} \cdot \mathbf{R}$  可以通过第一、第二基本型表示:

$$\left. \begin{aligned} g_{\alpha\beta} &= a_{\alpha\beta} - 2x^3 b_{\alpha\beta} + (x^3)^2 b_{\alpha}^{\lambda} b_{\lambda\beta} \\ g_{\alpha 3} &= g_{3\alpha} = 0, \quad g_{33} = 1 \end{aligned} \right\} \quad (2.3)$$

$$\left. \begin{aligned} \text{记} \quad a &= |a_{\alpha\beta}| & g &= |g_{ij}| \\ \text{则} \quad g &= a\theta & \theta &= 1 - 2Hx^3 + K(x^3)^2 \end{aligned} \right\} \quad (2.4)$$

其中  $H$ ,  $K$  分别为曲面  $S$  之平均曲率和全曲率

$$\mathbf{n} = \frac{\mathbf{R}_1 \times \mathbf{R}_2}{\sqrt{g}} = \frac{\mathbf{r}_1 \times \mathbf{r}_2}{\sqrt{a}} \quad (2.5)$$

这说明曲面  $\hat{S}: x^3 = \text{const}$  和  $S$  具有同样的法线。

逆变度量张量

$$\left. \begin{aligned} g^{\alpha\beta} &= \theta^{-2} \bar{b}_{\alpha}^{\lambda} \bar{b}_{\lambda\beta}, \quad g^{\alpha 3} = g^{3\alpha} = 0, \quad g^{33} = 1 \\ \bar{b}_{\beta}^{\alpha} &= (1 - 2Hx^3) \delta_{\beta}^{\alpha} + x^3 b_{\beta}^{\alpha} \end{aligned} \right\} \quad (2.6)$$

记  $\Gamma_{\alpha\beta}^{\lambda}$ ,  $\Gamma_{\alpha\beta,\lambda}$  为曲面  $S$  之第二, 第一 Christoffel 记号, 而  $G_{ij}^k$ ,  $G_{ij,k}$  记空间的第二, 第一 Christoffel 记号, 那么它们之间有如下关系。

$$\left. \begin{aligned} G_{\alpha\beta,\lambda} &= \Gamma_{\alpha\beta,\lambda} - x^3 (\nabla_{\beta} b_{\alpha\lambda} + 2\Gamma_{\alpha\beta}^{\sigma} b_{\sigma\lambda}) + (x^3)^2 (b_{\lambda}^{\sigma} \nabla_{\beta} b_{\alpha\sigma} + \Gamma_{\sigma\beta}^{\gamma} b_{\lambda\sigma} b_{\alpha}^{\gamma}) \\ G_{\alpha\beta,3} &= -G_{\alpha 3,\beta} = b_{\alpha\beta} - x^3 b_{\alpha}^{\lambda} b_{\lambda\beta} \\ G_{\alpha 3,3} &= 0, \quad G_{33,k} = 0 \end{aligned} \right\} \quad (2.7)$$

$$\left. \begin{aligned} G_{\alpha}^{\lambda\sigma} &= g^{\lambda\sigma} G_{\alpha\beta,\sigma} = \Gamma_{\alpha}^{\lambda\sigma} - x^3 \nabla_{\beta} b_{\alpha}^{\lambda} - (x^3)^2 b_{\gamma}^{\lambda} b_{\beta}^{\gamma} - \dots \\ & \quad (\text{通项为 } -(x^3)^n b_{\gamma_1}^{\lambda} b_{\gamma_2}^{\gamma_1} \dots b_{\gamma_{n-1}}^{\gamma_{n-2}} \nabla_{\alpha} b_{\beta}^{\gamma_{n-1}}) \\ G_{\alpha 3}^{\beta} &= g^{\beta\sigma} G_{\alpha 3,\sigma} = b_{\alpha}^{\beta} - x^3 b_{\gamma}^{\beta} b_{\alpha}^{\gamma} - (x^3)^2 b_{\gamma_1}^{\beta} b_{\gamma_2}^{\gamma_1} b_{\alpha}^{\gamma_2} - \dots \\ G_{3\alpha}^{\beta} &= 0, \quad G_{33}^{\alpha} = 0, \quad G_{3\alpha}^3 = 0 \end{aligned} \right\} \quad (2.8)$$

其中  $\nabla_{\beta}$  表示曲面张量之一阶协变导数。

由于润滑流体区域  $\Omega$  限于一个狭窄的空间, 当我们取  $S_0$  作为基础曲面  $S$ , 那么在  $\Omega$  内,  $0 \leq x^3 \leq h$ , 并且一般都满足  $1 \pm K_1 h \approx 1$ ,  $1 \pm K_2 h \approx 1$ , 其中  $K$  是主曲率, 这时我们略去  $x^3$  高阶小量, 则(2.3), (2.6), (2.7), (2.8)变为

$$\left. \begin{aligned} g_{\alpha\beta} &= a_{\alpha\beta}, \quad g_{\alpha 3} = g_{3\alpha} = 0, \quad g_{33} = 1, \quad g = a \\ g^{\alpha\beta} &= a^{\alpha\beta}, \quad g^{\alpha 3} = g^{3\alpha} = 0, \quad g^{33} = 1 \end{aligned} \right\} \quad (2.9)$$

$$\left. \begin{aligned} G_{\alpha\beta,\lambda} &= \Gamma_{\alpha\beta,\lambda} - x^3 \nabla_{\beta} b_{\alpha\lambda}, \quad G_{\alpha\beta,3} = b_{\alpha\beta} \\ G_{\alpha 3,\beta} &= -b_{\alpha\beta}, \quad G_{\alpha 3,3} = 0, \quad G_{33,k} = 0 \end{aligned} \right\} \quad (2.10)$$

$$\left. \begin{aligned} G_{\alpha}^{\lambda\sigma} &= \Gamma_{\alpha}^{\lambda\sigma} - x^3 \nabla_{\beta} b_{\alpha}^{\lambda}, \quad G_{\alpha}^3 = b_{\alpha\beta} \\ G_{\alpha 3}^{\beta} &= -b_{\alpha}^{\beta}, \quad G_{\alpha 3}^3 = 0, \quad G_{3\alpha}^{\beta} = 0 \end{aligned} \right\} \quad (2.11)$$

尤其当  $S$  是球面或圆柱面时,  $\nabla_{\sigma} b_{\alpha}^{\lambda} = 0$ , 因而有

$$\left. \begin{aligned} G_{\alpha\beta,\lambda} &= \Gamma_{\alpha\beta,\lambda}, \quad G_{\alpha\beta,3} = b_{\alpha\beta}, \quad G_{\alpha 3,\beta} = -b_{\alpha\beta} \\ G_{\alpha 3,3} &= 0, \quad G_{33,k} = 0 \end{aligned} \right\} \quad (2.12)$$

$$\left. \begin{aligned} G_{\alpha\beta}^{\lambda} &= \Gamma_{\alpha\beta}^{\lambda}, \quad G_{\alpha\beta}^{\gamma} = b_{\alpha\beta}, \quad G_{\alpha\gamma}^{\beta} = -b_{\alpha}^{\beta} \\ G_{\alpha\gamma}^{\delta} &= 0, \quad G_{\gamma\delta}^{\alpha} = 0 \end{aligned} \right\} \quad (2.13)$$

任一矢量  $u$  可以表示为

$$u = u^{\alpha} R_{\alpha} + u^{\delta} n, \quad u_{\alpha} = a_{\alpha\beta} u^{\beta}$$

记  $\tilde{\nabla}$  为空间张量之一阶协变导数, 那么

$$\tilde{\nabla}_i u^j = \frac{\partial u^j}{\partial x^i} + G_{ik}^j u^k \quad (2.14)$$

将(2.11)代入(2.14)得

$$\left. \begin{aligned} \tilde{\nabla}_{\alpha} u^{\beta} &= \nabla_{\alpha} u^{\beta} - x^{\delta} \nabla_{\alpha} b_{\delta}^{\beta} u^{\delta} - b_{\alpha}^{\delta} u^{\delta} \\ \tilde{\nabla}_{\alpha} u^{\delta} &= \frac{\partial u^{\delta}}{\partial x^{\alpha}} + b_{\alpha\sigma} u^{\sigma} \\ \tilde{\nabla}_{\delta} u^{\alpha} &= \frac{\partial u^{\alpha}}{\partial x^{\delta}} - b_{\delta}^{\alpha} u^{\beta} \\ \tilde{\nabla}_{\delta} u^{\delta} &= \frac{\partial u^{\delta}}{\partial x^{\delta}} \end{aligned} \right\} \quad (2.15)$$

其中

$$\nabla_{\alpha} u^{\beta} = \frac{\partial u^{\beta}}{\partial x^{\alpha}} + \Gamma_{\alpha\sigma}^{\beta} u^{\sigma}$$

关于二阶张量的协变导数同样可以导出:

$$\tilde{\nabla}_k f^{ij} = \frac{\partial f^{ij}}{\partial x^k} + G_{km}^i f^{mj} + G_{km}^j f^{im}$$

对于  $f^{\alpha\beta}$ ,  $f^{\delta\delta}$  等分量, 在曲面张量场中, 视为一阶逆变张量和数量, 因而利用(2.11)可得

$$\left. \begin{aligned} \tilde{\nabla}_{\sigma} f^{\alpha\beta} &= \nabla_{\sigma} f^{\alpha\beta} - x^{\delta} (f^{\gamma\beta} \nabla_{\sigma} b_{\gamma}^{\alpha} + f^{\alpha\gamma} \nabla_{\sigma} b_{\gamma}^{\beta}) - b_{\sigma}^{\alpha} f^{\delta\beta} - b_{\sigma}^{\beta} f^{\alpha\delta} \\ \tilde{\nabla}_{\sigma} f^{\alpha\delta} &= \nabla_{\sigma} f^{\alpha\delta} - x^{\beta} f^{\beta\gamma} \nabla_{\sigma} b_{\gamma}^{\alpha} + b_{\sigma\beta} f^{\alpha\beta} - b_{\sigma}^{\alpha} f^{\delta\delta} \\ \tilde{\nabla}_{\sigma} f^{\delta\alpha} &= \nabla_{\sigma} f^{\delta\alpha} - x^{\beta} f^{\beta\gamma} \nabla_{\sigma} b_{\gamma}^{\alpha} + b_{\sigma\beta} f^{\beta\alpha} - b_{\sigma}^{\alpha} f^{\delta\delta} \\ \tilde{\nabla}_{\sigma} f^{\delta\delta} &= \nabla_{\sigma} f^{\delta\delta} + b_{\sigma\alpha} (f^{\delta\alpha} + f^{\alpha\delta}) \\ \tilde{\nabla}_{\delta} f^{\alpha\beta} &= \frac{\partial f^{\alpha\beta}}{\partial x^{\delta}} - b_{\delta}^{\alpha} f^{\alpha\beta} - b_{\delta}^{\beta} f^{\alpha\delta} \\ \tilde{\nabla}_{\delta} f^{\delta\alpha} &= \frac{\partial f^{\delta\alpha}}{\partial x^{\delta}} - b_{\delta}^{\alpha} f^{\delta\alpha} \\ \tilde{\nabla}_{\delta} f^{\alpha\delta} &= \frac{\partial f^{\alpha\delta}}{\partial x^{\delta}} - b_{\delta}^{\alpha} f^{\delta\alpha} \\ \tilde{\nabla}_{\delta} f^{\delta\delta} &= \frac{\partial f^{\delta\delta}}{\partial x^{\delta}} \end{aligned} \right\} \quad (2.16)$$

如果我们利用曲面论公式

$$\left. \begin{aligned} b_{\alpha}^{\alpha} &= a^{\alpha\beta} b_{\beta\alpha} = 2H \\ \nabla_{\alpha} b_{\beta\sigma} - \nabla_{\sigma} b_{\beta\alpha} &= 0 \\ b_1^1 b_2^2 - b_2^1 b_1^2 &= K \end{aligned} \right\} \quad (2.17)$$

其中  $H$  为曲面  $S$  之平均曲率,  $K$  为全曲率或 Gauss 曲率; 那么可以推出

$$\nabla a b_{\sigma}^{\alpha} = \nabla \sigma b_{\sigma}^{\alpha} = 2 \nabla \sigma H \quad (2.18)$$

对(2.16)进行指标缩并, 并利用(2.17), (2.18)得

$$\begin{aligned} \tilde{\nabla}_{\nu} f^{i\alpha} &= \tilde{\nabla}_{\sigma} f^{\sigma\alpha} + \tilde{\nabla}_{\beta} f^{\beta\alpha} = \nabla_{\sigma} f^{\sigma\alpha} - x^{\beta} [2 f^{\sigma\alpha} \nabla_{\sigma} H + f^{\sigma\beta} \nabla_{\sigma} b_{\beta}^{\alpha}] \\ &\quad - 2 H f^{\beta\alpha} - b_{\sigma}^{\alpha} (f^{\sigma\beta} + f^{\beta\sigma}) + \frac{\partial f^{\beta\alpha}}{\partial x^{\beta}} \end{aligned} \quad (2.19)$$

$$\tilde{\nabla}_{\nu} f^{i\beta} = \tilde{\nabla}_{\sigma} f^{\sigma\beta} + \tilde{\nabla}_{\alpha} f^{\alpha\beta} = \nabla_{\sigma} f^{\sigma\beta} - 2 x^{\alpha} f^{\sigma\beta} \nabla_{\sigma} H + b_{\sigma\beta} f^{\sigma\alpha} - 2 H f^{\alpha\beta} + \frac{\partial f^{\alpha\beta}}{\partial x^{\alpha}} \quad (2.20)$$

尤其是, 下列二阶张量将是我们所感兴趣的:

$$f^{i\alpha} = \mu [g^{\alpha m} \tilde{\nabla}_m u^i + g^{mi} \tilde{\nabla}_m u^{\alpha}] \quad (2.21)$$

利用(2.15), (2.9)则(2.21)可以表示为

$$f^{\sigma\alpha} = \mu \{ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - x^{\beta} [ \nabla^{\sigma} b_{\beta}^{\alpha} + \nabla^{\alpha} b_{\beta}^{\sigma} ] u^{\beta} - 2 b^{\alpha\sigma} u^{\beta} \}$$

这里  $\nabla^{\sigma} \cdot = a^{\sigma\gamma} \nabla_{\gamma} \cdot$ , 如果利用(2.17), 那么

$$\nabla^{\sigma} b_{\beta}^{\alpha} + \nabla^{\alpha} b_{\beta}^{\sigma} = a^{\sigma\beta} \nabla_{\beta} b_{\gamma}^{\alpha} + a^{\alpha\beta} \nabla_{\beta} b_{\gamma}^{\sigma} = a^{\sigma\beta} \nabla_{\gamma} b_{\beta}^{\alpha} + a^{\alpha\beta} \nabla_{\gamma} b_{\beta}^{\sigma} = 2 \nabla_{\gamma} b^{\alpha\sigma}$$

故

$$\left. \begin{aligned} f^{\sigma\alpha} &= f^{\alpha\sigma} = \mu [ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - 2 x^{\beta} \nabla_{\gamma} b^{\alpha\sigma} u^{\beta} - 2 b^{\alpha\sigma} \cdot u^{\beta} ] \\ f^{\beta\alpha} &= f^{\alpha\beta} = \mu \left[ a^{\alpha\beta} \frac{\partial u^{\beta}}{\partial x^{\alpha}} + \frac{\partial u^{\alpha}}{\partial x^{\beta}} \right] \end{aligned} \right\} \quad (2.22)$$

将(2.22)代入(2.20)后, 得

$$\begin{aligned} \tilde{\nabla}_{\nu} f^{i\alpha} &= \nabla_{\sigma} \{ \mu [ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - 2 x^{\beta} \nabla_{\gamma} b^{\alpha\sigma} \cdot u^{\beta} - 2 b^{\alpha\sigma} \cdot u^{\beta} ] \} \\ &\quad - \mu x^{\beta} \{ 2 [ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - 2 x^{\gamma} \nabla_{\gamma} b^{\alpha\sigma} u^{\beta} - 2 b^{\alpha\sigma} \cdot u^{\beta} ] \nabla_{\sigma} H \\ &\quad + [ \nabla^{\beta} u^{\sigma} + \nabla^{\sigma} u^{\beta} - 2 x^{\gamma} \nabla_{\gamma} b^{\beta\sigma} \cdot u^{\gamma} - 2 b^{\beta\sigma} \cdot u^{\gamma} ] \nabla_{\sigma} b_{\beta}^{\alpha} \} \\ &\quad + \frac{\partial}{\partial x^{\beta}} \left\{ \mu \left( a^{\alpha\beta} \frac{\partial u^{\beta}}{\partial x^{\alpha}} + \frac{\partial u^{\alpha}}{\partial x^{\beta}} \right) \right\} - 2 \mu H \left\{ a^{\alpha\beta} \frac{\partial u^{\beta}}{\partial x^{\alpha}} + \frac{\partial u^{\alpha}}{\partial x^{\beta}} \right\} \\ &\quad - 2 \mu b_{\sigma}^{\alpha} \left[ a^{\sigma\beta} \frac{\partial u^{\beta}}{\partial x^{\alpha}} + \frac{\partial u^{\sigma}}{\partial x^{\beta}} \right] \end{aligned} \quad (2.23)$$

### 三、广义雷诺方程

在  $S_0$ ——坐标系下, 润滑流体所应满足的微分方程, 称为广义雷诺方程, 它考虑了曲线运动所产生的弯曲效应.

我们取  $x^{\beta}$  方向的平均值来代替原来的数值, 对于流体运动速度, 取

$$\bar{u} = \frac{1}{h} \int_0^h u dx^{\beta}$$

显然, 由(2.9)可推出:

$$\bar{\mathbf{u}} = \bar{u}^{\alpha} \mathbf{R}_{\alpha} + \bar{u}^{\beta} \mathbf{n}$$

其中  $\bar{u}^{\alpha} = \frac{1}{h} \int_0^h u^{\alpha} dx^{\beta}$ ,  $\bar{u}^{\beta} = \frac{1}{h} \int_0^h u^{\beta} dx^{\beta}$ , 由于  $\rho$  沿  $x^{\beta}$  方向变化很小,  $\bar{\rho} = \rho$  那么质量流量密度

$$\begin{aligned} \mathbf{q} &= \rho h \bar{u}^{\alpha} \mathbf{R}_{\alpha} = q^{\alpha} \mathbf{R}_{\alpha} \\ q^{\alpha} &= \rho h \bar{u}^{\alpha} = \rho \int_0^h u^{\alpha} dx^{\beta} \end{aligned} \quad (3.1)$$

## 3.1 连续性方程

$$\frac{\partial \rho}{\partial t} + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\frac{\partial \rho}{\partial t} + \frac{1}{\sqrt{g}} \frac{\partial}{\partial x^i} (\sqrt{g} \rho u^i) = 0$$

由于(2.9), 连续性方程可以表为

$$\frac{\partial \rho}{\partial t} + \frac{1}{\sqrt{a}} \frac{\partial}{\partial x^\alpha} (\sqrt{a} \rho u^\alpha) + \frac{\partial}{\partial x^3} (\rho u^3) = 0$$

沿着 $x^3$ 方向积分, 可以得到

$$\frac{\partial}{\partial t} (h\rho) + \frac{1}{\sqrt{a}} \frac{\partial}{\partial x^\alpha} (\sqrt{a} \rho u^\alpha) + \rho V_i^3 = 0 \quad (3.2)$$

其中  $u^3(0) = 0, \quad u^3(h) = V_i^3$

## 3.2 动量方程

Navier-Stokes 方程的张量形式

$$\frac{\partial u^i}{\partial t} + u^j \tilde{\nabla}_j u^i = X^i - \frac{1}{\rho} g^{ij} (\tilde{\nabla}_j (\rho - \lambda \operatorname{div} \mathbf{u}))$$

$$+ \frac{1}{\rho} g^{ek} \tilde{\nabla}_k [\mu g^{im} (\tilde{\nabla}_m u_e + \tilde{\nabla}_e u_m)] \quad (3.3)$$

其中 $u^i, u_i$ 分别为 $\mathbf{u}$ 之逆变分量和协变分量,  $\lambda, \mu$ 为粘性系数, 并且一般有

$$3\lambda + 2\mu = 0$$

$X^i$ 为体积力之逆变分量, 用 $u_i = g_{ij} u^j$ 代替, 并且注意到 $g_{ij}, g^{ij}$ 关于协变导数为零, 故

$$g^{ek} \tilde{\nabla}_k [\mu g^{im} (\tilde{\nabla}_m u_e + \tilde{\nabla}_e u_m)] = \tilde{\nabla}_k [\mu (g^{im} \tilde{\nabla}_m u^k + g^{ek} \tilde{\nabla}_j u^j)]$$

则(3.3)可以表示为

$$\frac{\partial u^i}{\partial t} + u^j \tilde{\nabla}_j u^i = X^i - \frac{1}{\rho} g^{ij} \tilde{\nabla}_j (p - \lambda \operatorname{div} \mathbf{u})$$

$$+ \frac{1}{\rho} \tilde{\nabla}_k [\mu (g^{im} \tilde{\nabla}_m u^k + g^{jk} \tilde{\nabla}_j u^i)] \quad (3.4)$$

当 $\lambda, \mu$ 为常数时, (3.4)可以表示为

$$\frac{\partial u^i}{\partial t} + u^j \tilde{\nabla}_j u^i = X^i - \frac{1}{\rho} g^{ij} \tilde{\nabla}_j (p - (\lambda + \mu) \operatorname{div} \mathbf{u}) + \frac{\mu}{\rho} g^{ek} \tilde{\nabla}_k \tilde{\nabla}_e u^i \quad (3.5)$$

如果流体是不可压,  $\operatorname{div} \mathbf{u} = 0$ , 则(3.4), (3.5)变为

$$\frac{\partial u^i}{\partial t} + u^j \tilde{\nabla}_j u^i = X^i - \frac{1}{\rho} g^{ij} \tilde{\nabla}_j p + \frac{1}{\rho} \tilde{\nabla}_k [\mu (g^{im} \tilde{\nabla}_m u^k + g^{ek} \tilde{\nabla}_e u^i)] \quad (3.6)$$

$$\frac{\partial u^i}{\partial t} + u^j \tilde{\nabla}_j u^i = X^i - \frac{1}{\rho} g^{ij} \tilde{\nabla}_j p + \frac{\mu}{\rho} g^{ek} \tilde{\nabla}_e \tilde{\nabla}_k u^i \quad (3.7)$$

利用表达式(2.21)及(2.9), 则(3.4)对于 $i$ 只取1, 2, 就有

$$\frac{\partial u^\alpha}{\partial t} + u^i \tilde{\nabla}_i u^\alpha = X^\alpha - \frac{1}{\rho} a^{\alpha\beta} \tilde{\nabla}_\beta (p - \lambda \operatorname{div} \mathbf{u}) + \frac{1}{\rho} \tilde{\nabla}_k f^{k\alpha}$$

略去惯 项和 $u^3$ , 则得

$$\begin{aligned}
 a^{\alpha\beta} \nabla_{\beta} (p - \lambda \operatorname{div} \mathbf{u}) &= \rho X^{\alpha} + \nabla_{\sigma} \{ \mu [ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - 2x^{\beta} \nabla_{\gamma} b^{\alpha\sigma} u^{\gamma} ] \} \\
 &\quad - 2\mu x^{\beta} \{ 2[ \nabla^{\alpha} u^{\sigma} + \nabla^{\sigma} u^{\alpha} - 2x^{\beta} \nabla_{\gamma} b^{\alpha\sigma} u^{\gamma} ] \nabla_{\sigma} H \\
 &\quad + [ \nabla^{\beta} u^{\sigma} + \nabla^{\sigma} u^{\beta} - 2x^{\beta} \nabla_{\gamma} b^{\sigma\beta} u^{\gamma} b_{\beta}^{\alpha} ] \nabla_{\sigma} b_{\beta}^{\alpha} \} \\
 &\quad + \frac{\partial}{\partial x^{\beta}} \left( \mu \frac{\partial u^{\alpha}}{\partial x^{\beta}} \right) - 2\mu H \frac{\partial u^{\alpha}}{\partial x^{\beta}} - 2\mu b_{\beta}^{\alpha} \frac{\partial u^{\sigma}}{\partial x^{\beta}} \quad (3.8)
 \end{aligned}$$

由于 $u^{\alpha}$ 随 $x^{\beta}$ 变化要比随 $x^{\beta}$ 变化小得多, 因而在略去 $u^{\alpha}$ 关于 $x^{\beta}$ 导数及 $x^{\beta}$ 的高阶无穷小量之后, (3.8) 可以表示为

$$\frac{\partial}{\partial x^{\beta}} \left( \mu \frac{\partial u^{\alpha}}{\partial x^{\beta}} \right) - 2\mu H \frac{\partial u^{\alpha}}{\partial x^{\beta}} - 2\mu b_{\beta}^{\alpha} \frac{\partial u^{\sigma}}{\partial x^{\beta}} = a^{\alpha\beta} \nabla_{\beta} p - \rho X^{\alpha} \quad (3.9)$$

$$\text{令} \quad y^{\alpha} = \mu \frac{\partial u^{\alpha}}{\partial x^{\beta}}, \quad f^{\alpha} = a^{\alpha\beta} \nabla_{\beta} p - \rho X^{\alpha}, \quad x^{\beta} = t \quad (3.10)$$

$$H_{\beta}^{\alpha} = 2(H\delta_{\beta}^{\alpha} + b_{\beta}^{\alpha}) \quad (3.11)$$

那么, (3.9) 可表示为

$$\frac{dy^{\alpha}}{dt} = H_{\beta}^{\alpha} y^{\beta} + f^{\alpha} \quad (3.12)$$

注意到(3.10), 积分上式, 并且 $H_{\beta}^{\alpha}$ ,  $f^{\alpha}$ 与 $t$ 无关, 因而

$$\frac{du^{\alpha}(t)}{dt} = \frac{du^{\alpha}(0)}{dt} + H_{\beta}^{\alpha} [u^{\beta}(t) - u^{\beta}(0)] + \frac{t}{\mu} f^{\alpha} \quad (3.13)$$

再积分一次

$$u^{\alpha}(t) = u^{\alpha}(0) + t \frac{du^{\alpha}(0)}{dt} + H_{\beta}^{\alpha} \left( \int_0^t u^{\beta}(\xi) d\xi - t u^{\beta}(0) \right) + \frac{t^2}{2\mu} f^{\alpha} \quad (3.14)$$

对(3.14)再从0到 $h$ 积分一次, 且两边乘 $\rho$ , 得

$$q^{\alpha} = h\rho u^{\alpha}(0) + \frac{\rho h^2}{2} \frac{du^{\alpha}(0)}{dt} + H_{\beta}^{\alpha} \left( \rho \int_0^h (h-\xi) u^{\beta}(\xi) d\xi - \frac{\rho h^2}{2} u^{\beta}(0) \right) + \frac{\rho h^3}{6\mu} f^{\alpha}$$

由于函数 $h-\xi$ 在 $(0, h)$ 单调下降, 且非负, 故运用积分第二中值定理

$$\rho \int_0^h (h-\xi) u^{\beta}(\xi) d\xi \approx h q^{\beta}$$

$$\text{故} \quad q^{\alpha} = h\rho u^{\alpha}(0) + \frac{\rho h^2}{2} \left( \frac{du^{\alpha}(0)}{dt} - H_{\beta}^{\alpha} u^{\beta}(0) \right) + h H_{\beta}^{\alpha} q^{\beta} + \frac{\rho h^3}{6\mu} f^{\alpha} \quad (3.15)$$

为了确定 $\frac{du^{\alpha}(0)}{dt}$ , 令(3.14)中 $t=h$ , 则

$$\begin{aligned}
 u^{\alpha}(h) &= u^{\alpha}(0) + h \frac{du^{\alpha}(0)}{dt} - H_{\beta}^{\alpha} \frac{q^{\beta}}{\rho} - h H_{\beta}^{\alpha} u^{\beta}(0) + \frac{h^2}{2\mu} f^{\alpha} \\
 \left( \frac{du^{\alpha}(0)}{dt} - H_{\beta}^{\alpha} u^{\beta}(0) \right) &= \frac{u^{\alpha}(h) - u^{\alpha}(0)}{h} - \frac{h}{2\mu} f^{\alpha} - \frac{1}{\rho h} H_{\beta}^{\alpha} q^{\beta} \quad (3.16)
 \end{aligned}$$

代入(3.15)得

$$q^{\alpha} = h\rho u^{\alpha}(0) + \frac{\rho h}{2} (u^{\alpha}(h) - u^{\alpha}(0)) - \frac{\rho h^3}{12\mu} f^{\alpha} + \left( \frac{h}{2} H_{\beta}^{\alpha} \right) q^{\beta} \quad (3.17)$$

将(3.11)代入(3.17)可得

$$A_{\beta}^{\alpha} q^{\beta} = -\frac{\rho h^3}{12\mu} f^{\alpha} + h \rho u^{\alpha}(0) + \frac{\rho h}{2} (u^{\alpha}(h) - u^{\alpha}(0)) \quad (3.18)$$

$$A_{\beta}^{\alpha} = \delta_{\beta}^{\alpha} - \frac{h}{2} H_{\beta}^{\alpha} = (1 - Hh) \delta_{\beta}^{\alpha} - hb_{\beta}^{\alpha}$$

令

$$A = \begin{vmatrix} A_1^1 & A_1^2 \\ A_2^1 & A_2^2 \end{vmatrix} = (1 - Hh - hb_1^1)(1 - Hh - hb_2^1) - h^2 b_1^2 b_2^1$$

利用(2.17)可得

$$A = (1 - Hh)(1 - 3Hh) - h^2 K = 1 - 4Hh + (3H^2 - K)h^2 \quad (3.19)$$

显然,  $A$  是一个不变量.

引入二阶张量

$$\begin{aligned} C^{11} = C^{22} = 0, & \quad C^{12} = -C^{21} = \frac{1}{\sqrt{a}} \\ C_{11} = C_{22} = 0, & \quad C_{12} = -C_{21} = \sqrt{a} \end{aligned}$$

和混合张量

$$B_{\beta}^{\alpha} = \frac{[(1 - Hh)\delta_{\beta}^{\alpha} - hC^{\alpha\gamma}C_{\beta\sigma}b_{\gamma}^{\sigma}]}{A} = \frac{[\delta_{\beta}^{\alpha} - h(H\delta_{\beta}^{\alpha} + C^{\alpha\gamma}C_{\beta\sigma}b_{\gamma}^{\sigma})]}{A} \quad (3.20)$$

那么, (3.18)的解可以表示为

$$q^{\alpha} = h \rho B_{\beta}^{\alpha} u^{\beta}(0) + \frac{1}{2} h \rho B_{\beta}^{\alpha} (u^{\beta}(h) - u^{\beta}(0)) - \frac{\rho h^3}{12\mu} B_{\beta}^{\alpha} f^{\beta}$$

代入(3.2)得

$$\begin{aligned} \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a} \rho h^3}{12\mu} B_{\beta}^{\alpha} f^{\beta} \right) &= \frac{\partial}{\partial x^{\alpha}} \left( \sqrt{a} h \rho B_{\beta}^{\alpha} u^{\beta}(0) \right) \\ &+ \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a}}{2} \rho h B_{\beta}^{\alpha} (u^{\beta}(h) - u^{\beta}(0)) \right) + \sqrt{a} \frac{\partial}{\partial t} (h\rho) + \sqrt{a} \rho V_{\beta}^{\beta} \end{aligned}$$

令  $V_{\beta}^{\beta} = u^{\beta}(h)$ ,  $U^{\alpha} = u^{\alpha}(0) = 0$  并将(3.10)代入, 得

$$\begin{aligned} \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a} \rho h^3}{12\mu} B_{\beta}^{\alpha} a^{\beta\sigma} \frac{\partial p}{\partial x^{\sigma}} \right) &= \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a} \rho^2 h^3}{12\mu} B_{\beta}^{\alpha} X^{\beta} \right) \\ &+ \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a}}{2} \rho h B_{\beta}^{\alpha} V_{\beta}^{\beta} \right) + \sqrt{a} \frac{\partial}{\partial t} (h\rho) + \sqrt{a} \rho V_{\beta}^{\beta} \end{aligned} \quad (3.21)$$

当  $U^{\alpha}$ ,  $U^{\beta}$  不为零时, (3.21) 可以写成

$$\begin{aligned} \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a} \rho h^3}{12\mu} B_{\beta}^{\alpha} a^{\beta\sigma} \frac{\partial p}{\partial x^{\sigma}} \right) &= \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a}}{12\mu} \rho^2 h^3 B_{\beta}^{\alpha} X^{\beta} \right) \\ &+ \frac{\partial}{\partial x^{\alpha}} \left[ \frac{\sqrt{a}}{2} \rho h B_{\beta}^{\alpha} (V_{\beta}^{\beta} - U^{\beta}) \right] + \sqrt{a} \frac{\partial}{\partial t} (h\rho) + \sqrt{a} \rho (V_{\beta}^{\beta} - U^{\beta}) \end{aligned} \quad (3.22)$$

当润滑流体是不可压时, 则(3.22)可以表示为

$$\begin{aligned} \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a} h^3}{12\mu} B_{\beta}^{\alpha} a^{\beta\sigma} \frac{\partial p}{\partial x^{\sigma}} \right) &= \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a}}{12\mu} \rho h^3 B_{\beta}^{\alpha} X^{\beta} \right) \\ &+ \frac{\partial}{\partial x^{\alpha}} \left( \frac{\sqrt{a}}{2} h B_{\beta}^{\alpha} (V_{\beta}^{\beta} - U^{\beta}) \right) + \sqrt{a} \frac{\partial}{\partial t} (h) + \sqrt{a} (V_{\beta}^{\beta} - U^{\beta}) \end{aligned} \quad (3.23)$$



它是压力  $p$  的线性椭圆型方程.

如果流体是理想气体, 则  $p = \rho RT$ , 那么(3.22)变为

$$\begin{aligned} \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a} h^3}{12\mu} B_\beta^\alpha a^{\beta\sigma} p \frac{\partial p}{\partial x^\sigma} \right) &= \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} h^3 B_\beta^\alpha X^\beta p^2 \right) / RT \\ &+ \frac{\partial}{\partial x^\alpha} \left[ \frac{\sqrt{a}}{2} h B_\beta^\alpha p (V_\beta^\beta - U^\beta) \right] + \sqrt{a} \frac{\partial}{\partial t} (h p) + \sqrt{a} p (V_\beta^\beta - U^\beta) \end{aligned} \quad (3.24)$$

它是压力  $p$  的拟线性椭圆型方程.

张量  $B_\beta^\alpha$  实际上是

$$B_1^1 = [1 - h(H + b_2^2)] / A$$

$$B_2^2 = -h b_1^1 / A$$

$$B_3^3 = -h b_1^1 / A$$

$$B_2^1 = [1 - h(H + b_1^1)] / A$$

令  $A^{\alpha\sigma} = B_\beta^\alpha a^{\beta\sigma}$ , 由于  $B_\beta^\alpha$  是  $h$  一次多项式,  $A$  是  $h$  的二次多项式, 且  $A|_{h=0} = 1$ , 而  $B_\beta^\alpha|_{h=0} = \delta_\beta^\alpha$ , 故

$$A^{\alpha\sigma}|_{h=0} = a^{\alpha\sigma} \quad (3.25)$$

因而, 如果欲使  $p$  的微分方程的主部只保持  $h$  的三次幂, 那么, (3.22)变为

$$\begin{aligned} \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a} \rho h^3}{12\mu} a^{\alpha\beta} \frac{\partial p}{\partial x^\beta} \right) &= \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} \rho h^3 X^\alpha \right) \\ &+ \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{2} h \rho (V_\beta^\beta - U^\alpha) \right) + \sqrt{a} \frac{\partial}{\partial t} (h \rho) + \rho \sqrt{a} (V_\beta^\beta - U^\beta) \end{aligned} \quad (3.26)$$

方程(3.22)或(3.26)称为广义雷诺方程, 它考虑了曲线运动所产生的弯曲效应, 与(1.1), (1.2)比较, 方程(3.22)更深刻地反映了轴瓦曲面的内蕴性质对润滑流动的影响, 在广义雷诺方程(3.22)的方程主部中和方程右端中, 均出现曲面  $S_0$  之第一、第二基本型, 平均曲率和全曲率.

当曲面  $S_0$  上的高斯坐标系取曲率线坐标系时

$$a_{12} = 0, \quad b_{12} = 0, \quad b_2^1 = b_1^2 = 0$$

$$b_{11} = K_1 a_{11}, \quad b_{22} = K_2 a_{22}, \quad K_1 = b_1^1, \quad K_2 = b_2^2$$

$K_1, K_2$  为主曲率, 因而

$$B_1^1 = [1 - h(H + K_2)] / A$$

$$B_2^2 = [1 - h(H + K_1)] / A$$

$$B_3^3 = B_1^1 = 0$$

在这种坐标系下

$$A^{11} = [1 - h(H + K_2)] a^{11} / A$$

$$A^{22} = [1 - h(H + K_1)] a^{22} / A$$

$$A^{12} = A^{21} = 0$$

这时方程(3.22)可表示为

$$\frac{\partial}{\partial x^1} \left( \frac{\sqrt{a} \rho h^3}{12\mu} \frac{1 - h(H + K_2)}{A} a^{11} \frac{\partial p}{\partial x^1} \right) + \frac{\partial}{\partial x^2} \left( \frac{\sqrt{a} \rho h^3}{12\mu} \frac{1 - h(H + K_1)}{A} a^{22} \frac{\partial p}{\partial x^2} \right)$$

$$\begin{aligned}
&= \frac{\partial}{\partial x^1} \left( \frac{\sqrt{a}}{12\mu} \rho^2 h^3 \frac{1-h(H+K_2)}{A} X^1 \right) + \frac{\partial}{\partial x^2} \left( \frac{\sqrt{a}}{12\mu} \rho^2 h^3 \frac{1-h(H+K_1)}{A} X^2 \right) \\
&+ \frac{\partial}{\partial x^1} \left[ \frac{\sqrt{a}}{2} \rho h \frac{1-h(H+K_2)}{A} (V_i^1 - U^1) \right] + \frac{\partial}{\partial x^2} \left[ \frac{\sqrt{a}}{2} \rho h \frac{1-h(H+K_1)}{A} (V_i^2 - U^2) \right] \\
&- U^2 \Big] + \sqrt{a} \frac{\partial}{\partial t} (h\rho) + \sqrt{a} \rho (V_i^3 - U^3) \quad (3.27)
\end{aligned}$$

边界条件分为两大类, 设  $\Gamma \equiv \partial\Omega = \Gamma_1 \cup \Gamma_2$ ,  $\Gamma_1$  为自由表面,  $\Gamma_2$  为固定表面, 于是

$$\begin{cases} p|_{\Gamma_2} = p_0 \\ \left[ \frac{h^3 \rho}{12\mu} \sqrt{a} B_i^\alpha a^{\lambda\beta} \nabla_\beta p \cdot n_\alpha + \frac{\sqrt{a}}{2} \rho h B_i^\alpha (V_i^\beta - U^\beta) \cdot n_\alpha \right] \Big|_{\Gamma_1} = g \end{cases} \quad (3.28)$$

其中  $n_\alpha$  为  $\mathbf{n}$  之协变分量.

如果油膜出现空泡现象, 设  $D \subset \Omega$  是流体占据的区域, 它是有界开集,  $\partial D \cap \Omega = \Gamma_c$ , 是空泡边界和  $\Omega$  的交集, 在  $\Gamma_c$  上,  $p$  应满足边界条件.

$$p|_{\Gamma_c} = 0, \quad \frac{\partial p}{\partial n} \Big|_{\Gamma_c} = 0 \quad (3.29)$$

我们的问题是在  $\Omega$  内求一个子集  $D$ , 使得在  $D$  内满足微分方程 (3.22), 在  $\Gamma_c$  上满足 (3.29), 在  $\Gamma_1 \cup \Gamma_2$  上满足 (3.28), 并且如果把大气压作为压力起点, 那么还应满足

$$p \geq 0 \quad (3.30)$$

#### 四、相应的不等变分问题

设  $V$  是  $H^1(\Omega)$  的子空间,  $V = \{u \in H^1(\Omega) \mid u|_{\Gamma_2} = 0\}$ , 那么, 对于  $V$  中的函数, 仍然成立 Friedrichs 不等式<sup>[1]</sup>:

$$\int_\Omega u^2 dx \leq C \int_\Omega |\nabla u|^2 dx \quad \forall u \in V$$

因而, 在  $V$  上, 范数  $\|\cdot\|$  和半范  $|u|_1 = |\nabla u|_2 = \left( \int_\Omega |\nabla u|^2 dx \right)^{1/2}$  是等价的, 我们可以记  $\|u\|_1^2 = |u|_1^2$ .

下面我们仅对方程 (3.22) 进行讨论. 先讨论不可压缩情形, 这时,  $p$  应满足 (3.22), 设

$$M^{\alpha\beta} = \frac{h^3}{12\mu} \sqrt{a} a^{\alpha\beta} \quad (4.1)$$

因为  $\nabla_\beta p = \frac{\partial p}{\partial x^\beta}$ , 在静态情形下, (3.22) 可以表示为

$$\begin{aligned}
\frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} \frac{\partial p}{\partial x^\beta} \right) &= \frac{\partial}{\partial x^\alpha} \left( \frac{h^3}{12\mu} \sqrt{a} \rho X^\alpha \right) + \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{2} \rho h (V_i^\alpha - U^\alpha) \right) \\
&+ \sqrt{a} \rho (V_i^3 - U^3) \quad (4.2)
\end{aligned}$$

设  $p_0 \in H^{3/2}(\Gamma_1)$ , 根据迹定理, 存在  $\hat{p}_0 \in H^2(\Omega)$ , 使得

$$\hat{p}_0|_{\Gamma_2} = p_0$$

令  $u = p - \hat{p}_0$ , 那么  $u|_{\Gamma_2} = 0$ , 故  $u \in V$ . 设  $U^i = 0$ , 代入 (4.2) 得

$$\frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} \frac{\partial u}{\partial x^\beta} + M^{\alpha\beta} \frac{\partial \bar{p}}{\partial x^\beta} - \frac{1}{2} \sqrt{a} h V_i^2 - \frac{h^3}{12\mu} \sqrt{a} \rho X^\alpha \right) - \sqrt{a} V_i^2 = 0 \quad (4.3)$$

设

$$f = \frac{\partial}{\partial x^\alpha} \left( -M^{\alpha\beta} \frac{\partial \bar{p}_0}{\partial x^\beta} \right) + \frac{1}{2} \sqrt{a} h (V_i^2 - U^2) + \frac{h^3}{12\mu} \sqrt{a} \rho X^\alpha + \sqrt{a} (V_i^2 - U^2) \quad (4.4)$$

则有

$$\left. \begin{aligned} \frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} \frac{\partial u}{\partial x^\beta} \right) &= f \\ M^{\alpha\beta} \frac{\partial u}{\partial x^\beta} n_\alpha |_{\Gamma_1} &= \bar{g} \end{aligned} \right\} \quad (4.5)$$

其中

$$\bar{g} = g - M^{\alpha\beta} \frac{\partial \bar{p}_0}{\partial x^\beta} n_\alpha |_{\Gamma_1} \quad (4.6)$$

作双线性泛函

$$a(u, v) = \int_\Omega M^{\alpha\beta} \frac{\partial u}{\partial x^\beta} \frac{\partial v}{\partial x^\alpha} dx \quad (4.7)$$

和线性泛函

$$\langle fg, v \rangle = \int_\Omega f v dx + \int_{\Gamma_1} \bar{g} v ds \quad (4.8)$$

因为  $S$  是二维曲面, 它的第一基本型  $a_{\alpha\beta}$  是对称正定的, 故  $M^{\alpha\beta}$  也是对称正定的

$$M^{\alpha\beta} \xi_\alpha \xi_\beta \geq C |\xi|^2, \quad \forall \xi \in R^2, \quad a \cdot e \cdot x^\alpha \in \Delta$$

故双线性泛函(4.7)是对称强制的:

$$a(u, u) \geq C_0 \|u\|^2$$

显然, 它也是有界的:

$$|a(u, v)| \leq M \|u\|_1 \cdot \|v\|_1$$

由于  $\bar{p}_0 \in H^2(\Omega)$ , 故可设  $f \in L^2(\Omega)$ ,  $\bar{g} \in H^{1/2}(\Gamma_1) \cup H^{-1/2}(\Gamma_2)$ , 由迹定理可知, 线性泛函(4.8)在  $V$  中有界:

$$\begin{aligned} |\langle fg, v \rangle| &\leq \|f\|_{L^2} \|v\|_{L^2} + \|\bar{g}\|_{H^{-1/2}(\Gamma_1)} \cdot \|v\|_{H^{-1/2}(\Gamma_1)} \\ &\leq (\|f\|_{L^2} + C \|\bar{g}\|_{H^{-1/2}(\Gamma_1)}) \|v\|_1 \end{aligned}$$

故  $fg \in V^*$  ( $V$  的对偶空间)。

设集合

$$K = \{v \in V \mid v|_{\Gamma_2} = \bar{p}_0, \quad a, e, \text{ 在 } \Delta \text{ 内}\} \quad (4.9)$$

显然  $K \subset V$  是一个闭凸集, 边值问题(4.5)是在  $K$  中求解, 即求  $u \in K$ , 使得  $u$  在  $\Delta$  上满足(4.5)

对应于(4.5)的能量泛函

$$J(u) = \frac{1}{2} a(u, u) - \langle fg, u \rangle \quad (4.10)$$

那么, (4.5)相应的Riesz变分问题是: 求  $u$ , 使得  $J(u)$  在  $K$  上达到极小值。

$$J(u) = \min_{v \in K} J(v) \quad (4.11)$$

我们知道, 当  $a(u, v)$  是对称、强制, 且是连续的, 那么, Riesz 极小化问题 (4.11) 等价于下列不等变分问题.

求  $u \in K$ , 使得

$$a(u, v-u) \geq \langle fg, v-u \rangle \quad \forall v \in K \quad (4.12)$$

对可压缩情形, 广义雷诺方程 (3.24) 是拟线性椭圆边值问题

$$\begin{aligned} \frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} p \frac{\partial p}{\partial x^\beta} \right) &= \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} h^3 X^\alpha \frac{p^2}{RT} \right) \\ &+ \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{2} h (V_i^\alpha - U^\alpha) p \right) + \sqrt{a} (V_i^\alpha - U^\alpha) p \end{aligned} \quad (4.13)$$

这里取  $B_i^\alpha = \delta_i^\alpha$ , 并考虑静态情形, 故  $M^{\alpha\beta} = \frac{\sqrt{a} h^3}{12\mu} a^{\alpha\beta}$  那么, 拟双线性泛函定义为

$$B(u, v) = \left( M^{\alpha\beta} u \frac{\partial u}{\partial x^\beta}, \frac{\partial v}{\partial x^\alpha} \right) \quad (4.14)$$

设

$$\begin{aligned} f(u) &= \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} \frac{h^3 X^\alpha}{RT} u^2 \right) + \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{2} h (V_i^\alpha - U^\alpha) u \right) \\ &+ \sqrt{a} (V_i^\alpha - U^\alpha) u \end{aligned} \quad (4.15)$$

则 (4.13) 可以表示为

$$\frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} u \frac{\partial u}{\partial x^\beta} \right) = f(u)$$

拟双线性泛函 (4.14) 在 Sobolev 空间  $H^{1,r}(\Omega)$   $r > 3$  中是连续和有界的, 实际上

$$\begin{aligned} |B(u, v)| &\leq \int \left| M^{\alpha\beta} \right| |u| \left| \frac{\partial u}{\partial x^\beta} \right| \left| \frac{\partial v}{\partial x^\alpha} \right| dx \\ &\leq C_1 \sum_{\beta=1}^2 \left\| u \frac{\partial u}{\partial x^\beta} \right\|_{L^{r'}(\Omega)} \|v\|_{H^{1,r}(\Omega)} \\ &\leq C_1 \sum_{\beta=1}^2 \|u\|_{L^{2r'}(\Omega)} \left\| \frac{\partial u}{\partial x^\beta} \right\|_{L^{2r'}(\Omega)} \|v\|_{H^{1,r}(\Omega)} \\ &\leq C_2 \|u\|_{H^{1,2r'}(\Omega)}^2 \|v\|_{H^{1,r}(\Omega)} \end{aligned}$$

这里  $\frac{1}{r} + \frac{1}{r'} = 1$ ,  $2r' = \frac{2r}{r-1}$  当  $r > 3$  时,  $r > 2r'$  由嵌入定理可知  $\|u\|_{H^{1,2r'}(\Omega)} \leq M \|u\|_{H^{1,r}(\Omega)}$ ,

故

$$|B(u, v)| \leq C_3 \|u\|_{H^{1,r}(\Omega)}^2 \|v\|_{H^{1,r}(\Omega)} \quad (4.16)$$

泛函  $f(u)$  在  $H^{1,r}(\Omega)$  同样是连续和有界的.

设  $W_0 \subset H^{1,r}(\Omega)$ ,  $W_0$  中的元素  $u$  在  $\Gamma_2$  上的迹为零,  $W_0$  的对偶空间记为  $W_0^*$ , 那么, 固定  $u \in W_0$ , 则  $B(u, v)$  是  $W_0$  上线性有界泛函, 故存在一个元素  $Tu \in W_0^*$ , 使得

$$B(u, v) = \langle Tu, v \rangle \quad (4.17)$$

且由 (4.16) 可知  $\|Tu\|_{W_0^*} \leq C_3 \|u\|_{H^{1,r}(\Omega)}^2$ ,  $Tu$  是一个从  $W_0 \rightarrow W_0^*$  的连续映照, 并且把  $W_0$  中有

界集映到  $W_0^1$  中的有界集.

设  $K \subset H^{1,r}(\Omega)$ , 使得

$$K = \{u \in H^{1,r}(\Omega) \mid u - \bar{p}_0 \in W_0, u > 0\} \quad (4.18)$$

那么,  $K$  是  $H^{1,r}(\Omega)$  中的一个凸集, 因而对于理想可压缩流体的广义雷诺方程边值问题

$$\left. \begin{aligned} \frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} u \frac{\partial u}{\partial x^\beta} \right) &= f(u) \\ u|_{r_2} &= p_0 \\ M^{\alpha\beta} u \frac{\partial u}{\partial x^\beta} n_\alpha|_{r_1} &= g \end{aligned} \right\} \quad (4.19)$$

它的广义解应满足不等变分问题: 求  $u \in K$ , 使得

$$B(u, v-u) \geq \langle f(u), v-u \rangle + \langle g, v-u \rangle_{r_1} \quad (4.20)$$

如果令  $P = u^2$ , 那么(4.19)可以写成

$$\left. \begin{aligned} \frac{\partial}{\partial x^\alpha} \left( M^{\alpha\beta} \frac{\partial P}{\partial x^\beta} \right) &= \tilde{f}(P) \\ P|_{r_2} &= \sqrt{p_0} \\ \frac{1}{2} M^{\alpha\beta} \frac{\partial P}{\partial x^\beta} n_\alpha|_{r_1} &= g \end{aligned} \right\} \quad (4.19)'$$

$$\begin{aligned} \text{其中} \quad \tilde{f}(P) &= 2 \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} h^3 \frac{X^\alpha}{RT} P \right) + 2 \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}h}{2} (V_\beta^\alpha - U^\alpha) \sqrt{P} \right) \\ &\quad + \sqrt{a} (V_\beta^\beta - U^\beta) \sqrt{P} \end{aligned} \quad (4.21)$$

对应于  $P$  的位势

$$\begin{aligned} F(P) &= \int_\Omega \left( \int_0^P \tilde{f}(x, \xi) d\xi \right) dx = \int_\Omega \left\{ \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{12\mu} \frac{h^3 X^\alpha}{RT} P^2 \right) \right. \\ &\quad \left. + \frac{\partial}{\partial x^\alpha} \left( \frac{\sqrt{a}}{3} h (V_\beta^\alpha - U^\alpha) P^{3/2} \right) + \frac{2}{3} \sqrt{a} (V_\beta^\beta - U^\beta) P^{3/2} \right\} dx \end{aligned} \quad (4.22)$$

那么, 对(4.19), 不等变分问题是: 求  $u \in K$  使

$$B(u, v-u) \geq \langle \text{grad } F(u), v-u \rangle + \langle g, v-u \rangle \quad \forall v \in K \quad (4.23)$$

其中  $B(u, v) = \int_\Omega M^{\alpha\beta} \frac{\partial u}{\partial x^\alpha} \frac{\partial v}{\partial x^\beta} dx$ ,  $\text{grad } F(u)$  是在点  $u$  的 Fréchet 导数.

不等变分问题的有限元逼近, 就是构造相应的有限元子空间  $S_h \subset V$  和闭凸集  $K_h \subset S_h \cap K$ , 那么

i) 求  $u_h \in K_h$ , 使得

$$J(u_h) = \min_{v_h \in K_h} J(v_h) \quad (4.24)$$

或 ii) 求  $u_h \in K_h$ , 使得

$$B(u_h, v_h - u_h) \geq \langle fg, v_h - u_h \rangle \quad \forall v_h \in K_h \quad (4.25)$$

通过有限元离散化, 我们知道  $J(u_h)$  是一个  $S_h$  上的二次型.

$$J(u_h) = \frac{1}{2} A_{ij} y^i y^j + C_i y^i = \frac{1}{2} Y^T A Y + Y^T C \quad (4.26)$$

其中系数矩阵  $A$  是正定对称和稀疏的, 因而(4.24)便成为一个大型对称正定稀疏的二次型数学规划问题, 可用规划理论求解.

线性和拟线性不等变分问题解的存在性已解决了<sup>[4][5]</sup>, 有限元解的误差估计和等变分问题有类似的结果<sup>[6]</sup>:

$$\|u - u_h\| \leq \left\{ \frac{M^2}{\gamma^2} \|u - v_h\|^2 + \frac{2}{\gamma^2} \|f - Tu\|^* (\|u - v_h\| + \|u_h - v_h\|) \right\}^{1/2}$$

其中  $M, \gamma$  常数是

$$\begin{aligned} |B(u, v)| &\leq M \|u\| \|v\| \\ B(u, u) &\geq \gamma \|u\|^2 \end{aligned}$$

$Tu$  是(4.17)中所定义的,  $u$  是真解,  $u_h$  是有限元逼近解,  $v \in V$  任一元素,  $v_h \in K_h$  任一元素, 对于非线性不等变分问题(4.22), 有限元逼近解的误差为

$$\begin{aligned} \|u - u_h\| &\leq \left\{ \frac{3M^2}{\gamma^2} (\|u - v_h\|^2 + \|v - u_h\|^2) + \frac{3M^2}{\gamma^2} \|v_h - v\|^2 \right. \\ &\quad \left. + \frac{2}{\gamma} (\|\text{grad } F(u)\|^* \|u - v_h\| + \|\text{grad } F(u_h) \right. \\ &\quad \left. - Tu_h\|^* \|u_h - v\|) \right\}^{1/2} \quad \forall v \in K, v_h \in K_h \end{aligned}$$

## 五、实 例

我们列举几种简单的轴承, 来看广义雷诺方程具有怎样的形式.

### 圆柱轴承

它的两个曲面  $S_0, S_1$  分别为圆柱面,  $S_0$  不动, 我们取  $z$  轴和它的轴重合,  $S_1$  以角速度  $\omega$  绕它自己的轴旋转, 我们取圆柱坐标系  $(x^1, x^2, x^3) = (r, \varphi, z)$ :

$$y^1 = r \cos \varphi, \quad y^2 = r \sin \varphi, \quad y^3 = z \quad (5.1)$$

$r = R$  为  $S_0$  曲面, 故取  $S_0$  上高斯坐标系为

$$x^1 = \varphi \quad x^2 = z \quad (5.2)$$

在圆柱坐标系下, 三维欧氏空间的度量张量  $g_{i'j'}$

$$\{g_{i'j'}\} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad (5.3)$$

那么,  $S_0$  曲面之度量张量

$$a_{\alpha\beta} = g_{i'j'} \frac{\partial x^{i'}}{\partial x^\alpha} \frac{\partial x^{j'}}{\partial x^\beta} \quad (5.4)$$

将(5.3)代入(5.4)得

$$\begin{aligned} [a_{\alpha\beta}] &= \begin{bmatrix} r^2 & 0 \\ 0 & 1 \end{bmatrix}, \quad a = r^2 \\ [a^{\alpha\beta}] &= \begin{bmatrix} 1/r^2 & 0 \\ 0 & 1 \end{bmatrix} \end{aligned} \quad (5.5)$$

设厚度为  $h$ ,  $R$  为轴承半径,  $r_1$  为轴径半径,  $e$  为偏心距,  $e = \frac{e}{R-r_1}$ , 那么不难验证

$$h = R - (r_1 + e \sin \varphi) = (R - r_1)(1 - \varepsilon \sin \varphi) \quad (5.6)$$

$S_b$  上切线速度  $\vec{v}_b$ ,  $v_b = r_1 \omega$

$$\vec{v}_b = V_b^\alpha \vec{e}_\alpha - V_b^3 \vec{n}$$

$$V_{b\alpha} = \vec{v}_b \cdot \vec{e}_\alpha$$

而

空间中任一点矢径  $\vec{R}$

$$\vec{R} = r \cos \varphi \vec{i} + r \sin \varphi \vec{j} + z \vec{k}$$

$$\vec{e}_\alpha = \frac{\partial \vec{R}}{\partial x^\alpha}$$

即

$$\vec{e}_1 = \frac{1}{R} [-r \sin \varphi \vec{i} + r \cos \varphi \vec{j}]$$

$$\vec{e}_2 = \vec{k}$$

故

$$V_{b2} = 0$$

$$V_{b3} = V_b^3 = \vec{v}_b \cdot \vec{n} = \omega e \sin \varphi$$

$$V_{b1} = \vec{v}_b \cdot \vec{e}_1 = \frac{1}{R} (r \sin \varphi \cdot r_1 \omega \sin \psi + r \cos \varphi \cdot r_1 \omega \cos \psi)$$

$$= \frac{r r_1}{R} \omega (\sin \varphi \sin \psi + \cos \varphi \cos \psi)$$

$$= \frac{r r_1}{R} \omega \cos (\varphi - \psi)$$

但  $r_1 \cos (\varphi - \psi) = R - (h + e \cos \varphi)$ ,  $r = R - h$  故

$$V_{b1} = R^2 \left(1 - \frac{h}{R}\right) \left(1 - \frac{h}{R} - \frac{e}{R} \cos \varphi\right) \omega$$

利用  $V_b^\alpha = a^{\alpha\beta} V_{b\beta}$  及 (5.5), 可知

$$V_b^1 = R^2 \left(1 - \frac{h}{R}\right) \left(1 - \frac{h}{R} - \frac{e}{R} \cos \varphi\right) \omega \frac{1}{r} = R \left(1 - \frac{h}{R} - \frac{e}{R} \cos \varphi\right) \omega$$

$$V_b^2 = 0$$

$$V_b^3 = -\omega e \sin \varphi, \quad U^1 = U^2 = U^3 = 0$$

不可压的广义雷诺方程 (3.22)

$$\frac{\partial}{\partial x^1} \left[ \frac{1}{R-h} \frac{h^3}{12\mu} \frac{\partial p}{\partial x^1} - \frac{1}{2} h R \left(1 - \frac{h}{R} - \frac{e}{R} \cos \varphi\right) \omega - \frac{h^3}{12\mu} \rho X^1 \right]$$

$$+ \frac{\partial}{\partial x^2} \left[ (R-h) \frac{h^3}{12\mu} \frac{\partial p}{\partial x^2} - \frac{h^3}{12\mu} \rho X^2 \right] - \frac{\partial h}{\partial t} - \omega e \sin \varphi = 0$$

椭圆柱轴承

同样取  $S_a$  之轴为  $z$  轴, 椭圆柱面坐标系  $(x^1, x^2, x^3) = (\eta, \varphi, z)$ , 那么

$$y^1 = a \operatorname{ch} \eta \cos \varphi, \quad y^2 = a \operatorname{sh} \eta \sin \varphi, \quad y^3 = z$$

则

$$[g_{i'j'}] = \begin{bmatrix} a^2 (\operatorname{ch}^2 \eta - \cos^2 \varphi) & 0 & 0 \\ 0 & a^2 (\operatorname{ch}^2 \eta - \cos^2 \varphi) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

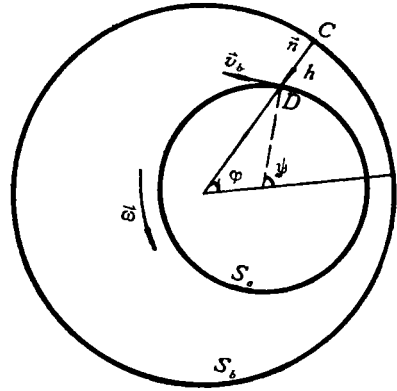


图 3

$$g_{1'1'} = \alpha^2(\operatorname{ch}^2\eta - \cos^2\varphi) = \alpha^2(\operatorname{sh}^2\eta + \sin^2\varphi) = g_{2'2'}$$

$$g_{s's'} = 1, \quad g_{i'j'} = 0 \quad (i' \neq j')$$

取

$$x^1 = \varphi, \quad x^2 = z$$

则

$$a_{\alpha\beta} = g_{i'j'} \frac{\partial x^{i'}}{\partial x^\alpha} \frac{\partial x^{j'}}{\partial x^\beta}$$

即有

$$a_{11} = \alpha^2(\operatorname{sh}^2\eta + \sin^2\varphi), \quad a_{22} = 1, \quad a_{12} = a_{21} = 0$$

$$a = \alpha^2(\operatorname{sh}^2\eta + \sin^2\varphi)$$

不可压缩的广义雷诺方程为

$$\begin{aligned} & \frac{\partial}{\partial x^1} \left( \frac{h^3}{12\mu\sqrt{a}} \frac{\partial p}{\partial x^1} \right) + \frac{\partial}{\partial x^2} \left( \frac{h^3\sqrt{a}}{12\mu} \frac{\partial p}{\partial x^2} \right) \\ &= \frac{\partial}{\partial x^\alpha} \left( \frac{1}{2} h\sqrt{a} V^\alpha + \frac{h^3}{12\mu} \rho\sqrt{a} X^\alpha \right) + \sqrt{a} \left( V_b^3 + \frac{\partial h}{\partial t} \right) \end{aligned}$$

### 旋转曲面

在圆柱坐标系中, 若  $r$  和  $z$  承受变换

$$r = r(u^1, u^2), \quad z = z(u^1, u^2)$$

那么, 曲线坐标系  $(u^1, u^2, \varphi)$  称为回转坐标系

$$y^1 = r(u^1, u^2) \cos \varphi, \quad y^2 = r(u^1, u^2) \sin \varphi, \quad y^3 = z(u^1, u^2)$$

对于旋转曲面, 我们采用回转坐标系, 尤其是对  $S_0$  测地超曲面, 其母线方程可以用自己的弧长  $m$  作参数

$$r = r(m), \quad z = z(m)$$

这时, 我们取  $(m, \varphi) = (x^1, x^2)$  作为  $S_0$  上高斯坐标系, 由于圆柱坐标系中, 三维欧氏空间度量张量为(5.3), 故

$$a_{\alpha\beta} = \frac{\partial r}{\partial x^\alpha} \frac{\partial r}{\partial x^\beta} + r^2 \frac{\partial \varphi}{\partial x^\alpha} \frac{\partial \varphi}{\partial x^\beta} + \frac{\partial z}{\partial x^\alpha} \frac{\partial z}{\partial x^\beta}$$

从而

$$a_{11} = \left( \frac{\partial r}{\partial m} \right)^2 + \left( \frac{\partial z}{\partial m} \right)^2 = 1, \quad a_{12} = a_{21} = 0$$

$$a_{22} = r^2, \quad a = r^2$$

$$a^{11} = 1, \quad a^{22} = \frac{1}{r^2}, \quad a^{12} = a^{21} = 0$$

所以广义雷诺方程为

$$\begin{aligned} & \frac{\partial}{\partial m} \left( \frac{h^3}{12\mu} \frac{1}{r} \frac{\partial p}{\partial m} - \frac{1}{2} hrV_b^1 - \frac{h^3}{12\mu} \rho r X^1 \right) \\ & + \frac{\partial}{\partial \varphi} \left( \frac{h^3}{12\mu} r \frac{\partial p}{\partial \varphi} - \frac{1}{2} hrV_b^2 - \frac{h^3}{12\mu} \rho r X^2 \right) - rV_b^3 - r \frac{\partial h}{\partial t} = 0 \end{aligned}$$

事实上, 曲面  $S_a$  和  $S_b$  不一定都要是规则曲面, 只要给出曲面的离散点, 同样可以很容易选取高斯坐标系和计算度量张量  $a_{\alpha\beta}$ .



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## Generalized Reynolds Equation and Variational Inequality in Lubrication Theory

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**Abstract**

This paper has derived generalized Reynolds equation in lubrication theory in terms of tensor analysis and  $S$ -coordinate system, and has provided corresponding variational inequality. The winding effect of flow of lubricant fluid is considered, and influence of inner properties of axis and axle sleeveings on the flow are counted.